

FACULDADE DE ENGENHARIA DA UNIVERSIDADE DO PORTO

DEPARTAMENTO DE ENGENHARIA DE MINAS

ESTUDO DOS PROCESSOS DE CLASSIFICAÇÃO DE CAULINOS NUMA INSTALAÇÃO INDUSTRIAL

ENSAIO DE INTERPRETAÇÃO DE DADOS OBTIDOS EM REGIME NÃO PERMANENTE

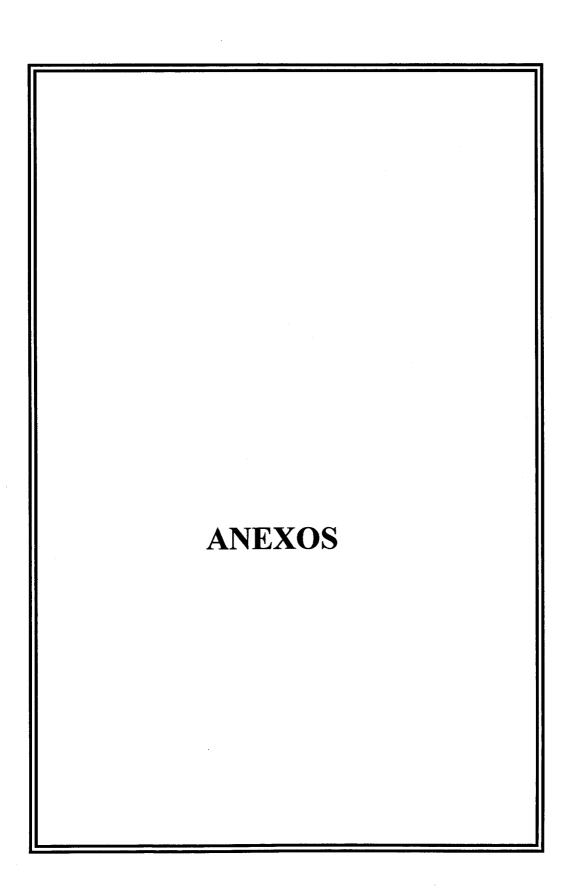
VOLUME DE ANEXOS

Dissertação para a obtenção de grau de mestre em Tecnologia e Gestão de Recursos Minerais

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(Fevereiro de 1996)



ANEXO I

DETERMINAÇÃO EXPERIMENTAL DE DADOS

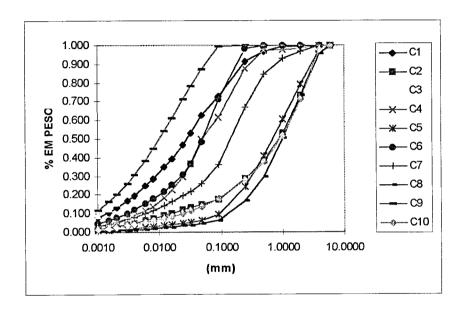
- AMOSTRAGEM 1
- HISTOGRAMA E CUMULANTE INFERIOR
- -CURVAS GRANULOMÉTRICAS CUMULANTES
- OUTPUTS DO COULTER
- AMOSTRAGEM 2
- HISTOGRAMA E CUMULANTE INFERIOR
- -CURVAS GRANULOMÉTRICAS CUMULANTES
- OUTPUTS DO COULTER
- AMOSTRAGEM 3
- HISTOGRAMA E CUMULANTE INFERIOR
- -CURVAS GRANULOMÉTRICAS CUMULANTES
- OUTPUTS DO COULTER
- PERCENTAGEM DE SÓLIDOS

AMOSTRAGEM 1, 2 E 3

AMOSTRAGEM Nº 1

guest en			Wat Alaman		ISTOGRAM	A Commence of the			n yek aktore et kanalan ye.	
(mm)	Ci	C2	C:3	C4	C5	C6	C7	C8	C9	C10
6.0000	0.000	0.021	0.000	0.000	0.019	0.000	0.000	0.045	0.000	0.022
4.0000	0.003	0.247	0.000	0.014	0.186	0.000	0.027	0.222	0.000	0.268
2.0000	0.002	0.202	0.000	0.008	0.190	0.000	0.049	0.226	0.000	0.193
1.0000	0.004	0.147	0.000	0.005	0.196	0.002	0.091	0.207	0.000	0.137
0.5000	0.017	0.098	0.003	0.007	0.164	0.014	0.195	0.127	0.000	0.099
0.2500	0.162	0.107	0.072	0.147	0.151	0.269	0.308	0.106	0.005	0.098
0.0900	0.183	0.028	0.147	0.321	0.028	0.230	0.069	0.019	0.126	0.043
0.0480	0.099	0.017	0.107	0.132	0.011	0.119	0.040	0.008	0.089	0.023
0.0320	0.060	0.013	0.073	0.066	0.006	0.055	0.025	0.005	0.069	0.014
0.0240	0.074	0.018	0.094	0.074	0.008	0.057	0.031	0.006	0.099	0.017
0.0160	0.047	0.012	0.062	0.042	0.005	0.034	0.020	0.004	0.070	0.011
0.0120	0.062	0.017	0.081	0.046	0.007	0.042	0.027	0.005	0.097	0.013
0.0080	0.039	0.011	0.051	0.024	0.004	0.025	0.016	0.003	0.061	800.0
0.0060	0.049	0.014	0.065	0.026	0.005	0.031	0.021	0.004	0.078	0.011
0.0040	0.031	0.009	0.040	0.015	0.003	0.019	0.013	0.002	0.048	0.007
0.0030	0.037	0.010	0.048	0.017	0.004	0.023	0.015	0.003	0.058	800.0
0.0020	0.023	0.006	0.029	0.010	0.002	0.014	0.009	0.002	0.036	0.005
0.0015	0.030	0.007	0.036	0.013	0.003	0.018	0.012	0.002	0.046	0.006
0.0010	0.079	0.017	0.093	0.034	0.008	0.048	0.031	0.005	0.119	0.016
SUM	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
				S. E.L.	ENDER!	= 7.• 37				
(mm)	C1	C2	C3	C4	C5	C6	C7	C8	C9	C10
6,0000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
4.0000	1.000	0.979	1.000	1.000	0.981	1.000	1.000	0.955	1.000	0.978
2.0000	0.997	0.733	1.000	0.986	0.794	1.000	0.973	0.733	1.000	0.710
1.0000	0.996	0.530	1.000	0.978	0.604	1.000	0.924	0.506	1.000	0.518
0.5000	0.991	0.383	1.000	0.973	0.408	0.998	0.834	0.299	1.000	0.380
0.2500	0.974	0.285	0.997	0.966	0.244	0.984	0.639	0.172	1.000	0.281
0.0740	0.812	0.178	0.925	0.819	0.094	0.715	0.331	0.066	0.995	0.183
0.0480	0.629	0.150	0.779	0.498	0.066	0.485	0.261	0.047	0.870	0.140
0.0320	0.530	0.133	0.672	0.366	0.055	0.366	0.221	0.039	0.781	0.117
0.0240	0.470	0.120	0.599	0.300	0.049	0.311	0.196	0.035	0.712	0.103
0.0160	0.396	0.103	0.505	0.226	0.041	0.254	0.165	0.029	0.613	0.086
0.0120	0.349	0.090	0.443	0.184	0.036	0.220	0.145	0.025	0.543	0.075
0.0080	0.287	0.074	0.362	0.138	0.030	0.178	0.118	0.021	0.446	0.062
0.0060	0.249	0.063	0.311	0.115	0.026	0.153	0.101	0.018	0.385	0.053
0.0040	0.199	0.049	0.246	0.088	0.020	0.122	0.081	0.014	0.307	0.043
0.0030	0.169	0.041	0.205	0.073	0.017	0.102	0.068	0.011	0.259	0.036
0.0020	0.132	0.030	0.158	0.057	0.013	0.080	0.052	0.008	0.201	0.028
0.0015	0.109	0.024	0.129	0.047	0.011	0.066	0.043	0.007	0.165	0.022
0.0010	0.079	0.017	0.093	0.034	800.0	0.048	0.031	0.005	0.119	0.016

CURVAS GRANULOMÉTRICAS DOS PRODUTOS RESULTANTES DA 1ª AMOSTRAGEM



Run 1 of 1

File name:

3/5/94 Group ID: Run number: 2

Sample ID: Operator:

nº1

Comments: Start time:

11:29 6 Jan 1995

Pump Speed:

75

Obscuration:

10% Optical model: Fraunhofer LS 130 Fluid modul

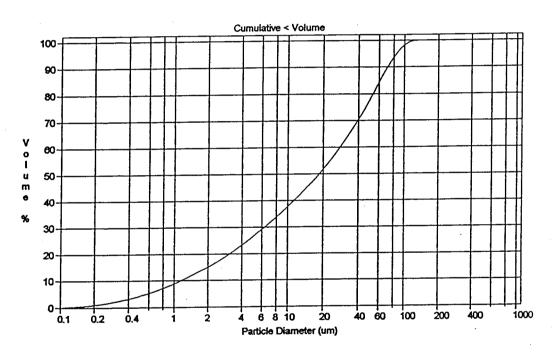
Software:

1.53

Fluid module Firmware:

1.3 1.8

Run length: 60 Seconds



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean:

28.18 um 18.48 um 95% Conf. Limits: 0-82.9 um

S.D.:

27.9 um

Median: Mean/Median Ratio: 1.525

Variance: C.V.:

779 um²

Mode:

56.00 um

99.1%

Skewness: Kurtosis:

1.04 Right skewed 0.268 Leptokurtic

Size um 1.156

25 4.527

50 18.48 45.90

75

Run 1 of 1

3/5/94

1.3 1.8

File name:

Group ID:

n*2 Sample ID:

Operator:

Comments:

11:07 5 Jan 1995 Start time:

Pump Speed: 75

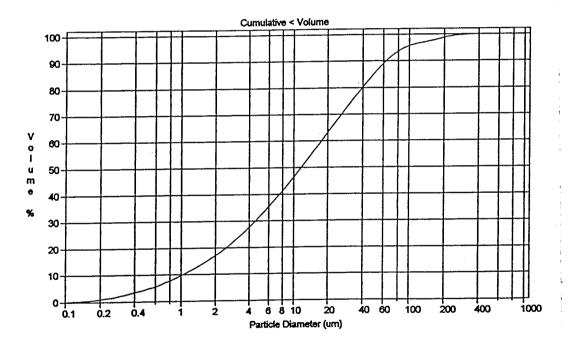
Software:

Run number: 1

Run length: 61 Seconds

11% Obscuration: Optical model: Fraunhofer LS 130 Fluid module





Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume Mean:

100.0%

25.74 um

95% Conf. Limits: 0-103 um

Median:

11.64 um

S.D.:

39.3 um

Mean/Median Ratio: 2.211

Variance: C.V.:

1540 um²

Mode:

24.68 um

153%

Skewness:

3.45 Right skewed

Kurtosis:

15.4 Leptokurtic

% < 10 Size um 1.042

25 3.435

50 11.64

32.11

Run 1 of 1

File name:

3/5/94 Group ID:

Sample ID: Operator:

n*3

Comments:

LS 130

Software:

12:01 6 Jan 1995

Run number: 4 Run length: 61 Seconds

Start time: Pump Speed: Optical model:

75 Obscuration:

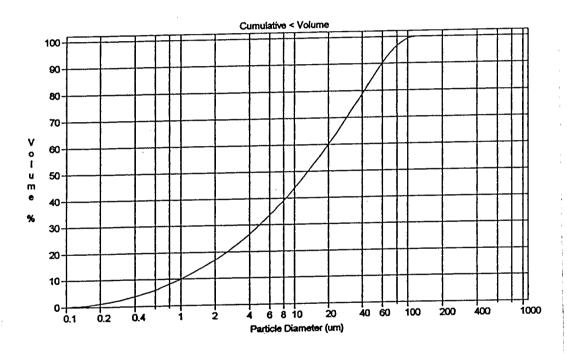
13%

Fraunhofer Fluid module

1.53

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume Mean:

100.0%

22.51 um 13.18 um

95% Conf. Limits: 0-89.6 um

Median: Mean/Median Ratio: 1.709

S.D.:

24 um $577\,\mathrm{um}^2$

Variance:

Mode:

42.62 um

C.V.:

107%

Skewness: Kurtosis:

1.32 Right skewed

1.14 Leptokurtic

10 % < Size um 0.999

3.628

50 13.18 75 34.87

Run 1 of 1

3/5/94

File name: Sample ID:

Operator:

Comments: Start time:

11:12 6 Jan 1995

Pump Speed: 75

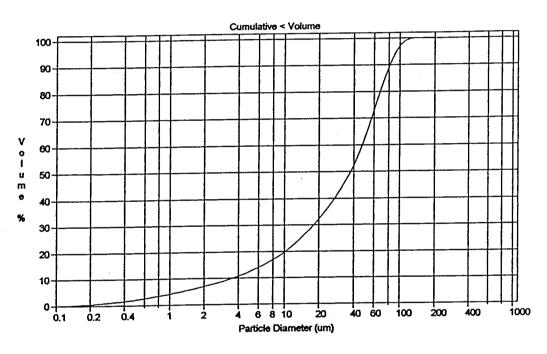
Group ID:

Run number: 1

Run length: 61 Seconds

1.3 1.8 Firmware:

11% Obscuration: Optical model: Fraunhofer LS 130 Fluid module Software: 1.53



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean:

40.32 um

95% Conf. Limits: 0-98.1 um S.D.:

Median:

37.41 um

29.5 um

Mean/Median Ratio: 1.078

Variance:

Kurtosis:

870 um²

Mode:

61.34 um C.V.: 73.2%

Skewness:

0.467 Right skewed -0.652 Platykurtic

10 % < Size um 3.563 25 13.91

50 37.41 75 62.16 81.80

90

11:48 6 Jan 1995

Run 1 of 1

3/5/94

File name:

Sample ID:

Group ID:

Operator:

Comments:

11:46 6 Jan 1995

Start time: Pump Speed:

10%

Obscuration: Optical model: Fraunhofer

Fluid module

LS 130 Software:

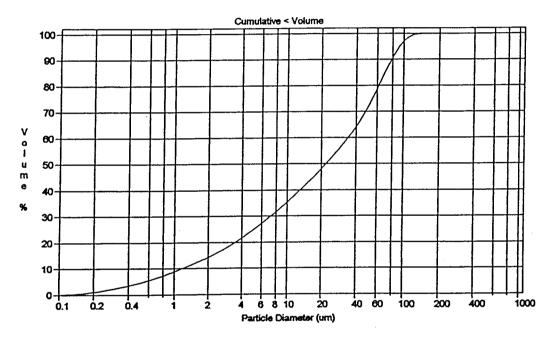
1.53

Run number: 3

Run length: 60 Seconds

1.3 1.8

Firmware:



Volume Statistics (Arithmetic)

(Untitled)

alculations from 0.100 um to 900.0 um

olume

100.0%

lean: ledian:

32.34 um 22.02 um lean/Median Ratio: 1.469

S.D.:

95% Conf. Limits: 0-92.9 um 30.9 um

954 um²

67.19 um

Variance: C.V.: Skewness:

95.5% 0.857 Right skewed

Kurtosis:

-0.229 Platykurtic

Size um 1.172

25 5.138

50 22.02

54.78

11:58 11 Jan 19

Run 1 of 1

3/5/94

File name:

Sample ID: 6 Group ID:

Operator:

Comments: Start time:

11:56 11 Jan 1995

75

Pump Speed: Obscuration:

11%

Optical model: Fraunhofer

Fluid module

LS 130 Software:

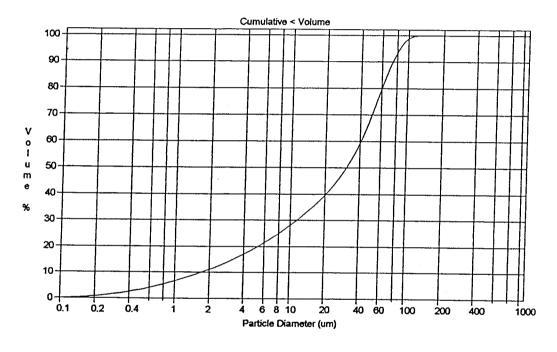
1.53

Run number: 3

Run length: 61 Seconds

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean: Median: 34.26 um

30.83 um

95% Conf. Limits:

S.D.:

0-88.6 um 27.7 um

Mean/Median Ratio: 1.112

Variance:

767 um²

Mode:

56.00 um

C.V.:

Skewness:

80.8%

Kurtosis:

0.537 Right skewed

-0.66 Platykurtic

% < 10 Size um 1.695

8.049

30.83

54.98

11:44 5 Jan 199

Run 1 of 1

3/5/94

File name:

n•7

Group ID: Run number: 3

Sample ID: Operator:

Comments:

Start time: 11:42 5 Jan 1995

Pump Speed: 75

Obscuration: 10% Optical model: Fraunhofer LS 130 Fluid model

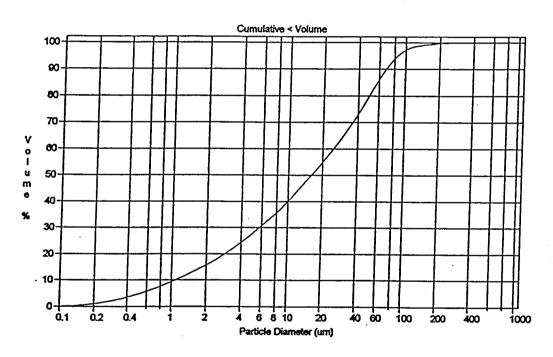
Software:

Fluid module

1.53

Firmware: 1.3 1.8

Run length: 61 Seconds



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean; 27.50 um Median: 16.05 um

95% Conf. Limits: 0-88.9 um S.D.: 31.3 um

Mean/Median Ratio: 1.713

Variance:

Mode:

51.13 um

C.V.:

961 um² 114%

Skewness:

2.12 Right skewed

Kurtosis:

7.38 Leptokurtic

% ₹

10 Size um 1.085

4.178

16.05

42.37

COULTERR LS Particle Size Analysis

11:21 11 Jan 19:

Run 1 of 1

File name: Sample ID:

8

Group ID: 3/5

Operator:

Run number: 1

Comments: Start time:

11:19 11 Jan 1995 Pump Speed: 75

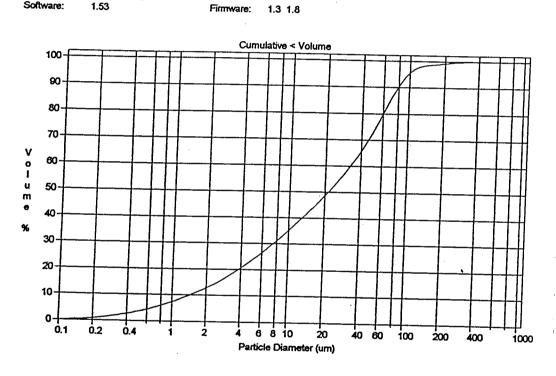
Obscuration: Optical model: Fraunhofer LS 130 Fluid modul

10%

Software:

Fluid module 1.53

Run length: 61 Seconds



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume Mean:

100.0%

Median:

33.67 um

61.34 um

21.34 um

95% Conf. Limits: 0-107 um S.D.:

37.3 um

Mean/Median Ratio: 1.577 Mode:

Variance:

1390 um²

C.V.:

111%

Skewness:

2.26 Right skewed

Kurtosis:

8.82 Leptokurtic

% < ` % < 10 Size um 1.442

5.452

21.34

75 52.58

Run 1 of 1 3/5/94

File name:

n*9

Sample ID: Operator:

Comments:

Start time:

11:24 5 Jan 1995 Pump Speed: 75

11% Obscuration:

Optical model: Fraunhofer LS 130

Software:

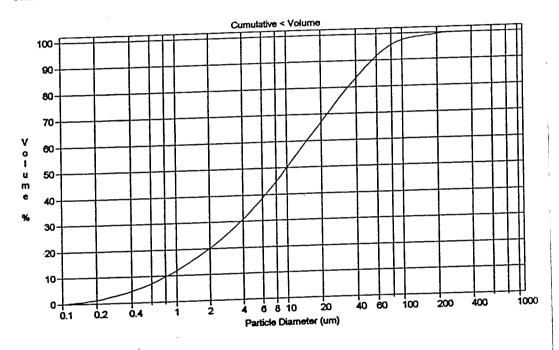
Fluid module 1.53

Group ID: Run number: 2

Run length: 61 Seconds

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

- Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean:

21.20 um

S.D.:

95% Conf. Limits: 0-80.8 um 30.4 um

9,968 um Median:

Variance:

924 um²

Mean/Median Ratio: 2.127
Mode: 11.91 um Mode:

C.V.:

143%

Skewness:

3,25 Right skewed

Kurtosis:

15 Leptokurtic

10 Size um 0.826 25 2.818

50% 9.968 75 27.72

Run 1 of 1

3/5/94

File name:

Sample ID: Operator:

10

75 15%

Comments:

Start time:

12:11 11 Jan 1995

Pump Speed:

Obscuration:

Optical model: Fraunhofer LS 130 Fluid modul

Software:

Fluid module

1.53

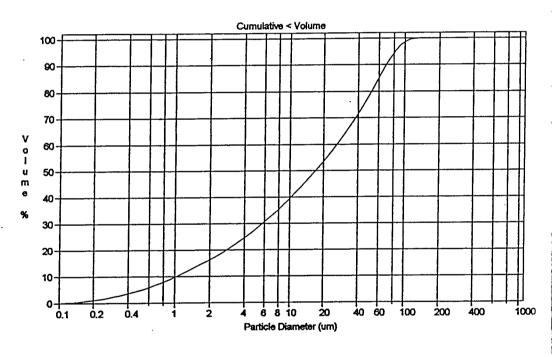
Firmware:

Group ID:

Run number: 4

Run length: 60 Seconds

1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean: Median: 27.08 um

16.97 um

S.D.:

95% Conf. Limits: 0-80.6 um 27.3 um

Mean/Median Ratio: 1.596 Mode:

Variance:

747 um²

56.00 um

C.V.:

101%

Skewness: Kurtosis:

1.05 Right skewed

10 % <

44.60

0.26 Leptokurtic

Size um 1.030

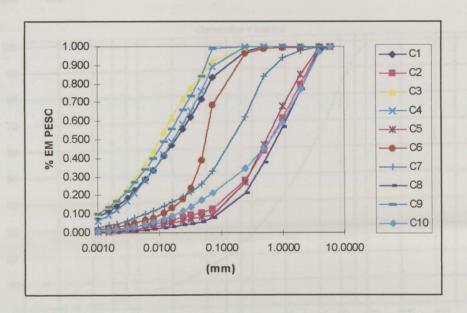
25 4.132

50 16.97

AMOSTRAGEM N° 2

	: STOCKANA							en time de la servició de la companya de la company	Commence of the second		
(mm)	C1	C2	C3	C4	C5	C6	C7	C8	C9	C10	
6.0000	0.000	0.006	0.000	0.000	0.005	0.000	0.000	0.016	0.000	0.025	
4.0000	0.000	0.198	0.000	0.000	0.146	0.003	0.021	0.212	0.000	0.206	
2.0000	0.000	0.180	0.000	0.000	0.171	0.001	0.039	0.204	0.000	0.174	
1.0000	0.001	0.174	0.001	0.000	0.204	0.004	0.102	0.193	0.000	0.143	
0.5000	0.023	0.158	0.006	0.002	0.203	0.027	0.216	0.163	0.000	0.108	
0.2500	0.140	0.156	0.074	0.107	0.174	0.277	0.294	0.132	0.009	0.130	
0.0740	0.119	0.019	0.070	0.132	0.015	0.301	0.070	0.023	0.150	0.040	
0.0480	0.096	0.015	0.071	0.102	0.011	0.149	0.041	0.011	0.106	0.038	
0.0320	0.065	0.010	0.062	0.072	0.009	0.055	0.024	0.007	0.075	0.022	
0.0240	0.085	0.014	0.098	0.096	0.012	0.049	0.029	0.008	0.101	0.025	
0.0160	0.059	0.009	0.077	0.066	0.009	0.026	0.020	0.005	0.069	0.015	
0.0120	0.077	0.013	0.108	0.088	0.011	0.027	0.027	0.007	0.091	0.018	
0.0080	0.048	0.008	0.067	0.054	0.006	0.014	0.017	0.004	0.057	0.010	
0.0060	0.061	0.010	0.083	0.068	0.007	0.016	0.021	0.004	0.073	0.012	
0.0040	0.038	0.006	0.050	0.042	0.004	0.009	0.013	0.002	0.045	0.007	
0.0030	0.044	0.007	0.056	0.049	0.004	0.010	0.016	0.002	0.053	0.007	
0.0020	0.027	0.004	0.033	0.028	0.002	0.006	0.010	0.001	0.032	0.004	
0.0015	0.034	0.004	0.041	0.031	0.002	0.007	0.013	0.001	0.040	0.005	
0.0010	0.084	0.009	0.103	0.063	0.005	0.019	0.028	0.004	0.100	0.012	
SUM	4	1.000	4 666	4 666	1.000	4 66	4.000	4 000	4.000		
	1.000		1.000	1.000		1.000	1.000	1.000	1.000	1.000	
SUM	7 5 9 4 1 5				en grann					1.000	
(mm)	1	2	3	4	SHUTAN) 5	6	7	8	9	1.000	
(mm) 6.0000	1 1.000	2 1.000	3 1.000	4 1.000	5 1.000	6 1.000	7	8	9		
(mm) 6.0000 4.0000	1 1.000 1.000	2 1.000 0.994	3 1.000 1.000	4 1.000 1.000	5 1,000 0,995	6 1.000 1.000	7 1.000 1.000	8 1.000 0.984	9 1.000 1.000	10	
(mm) 6.0000 4.0000 2.0000	1 1.000 1.000 1.000	2 1.000 0.994 0.796	3 1.000 1.000 1.000	4 1.000 1.000 1.000	5 1.000 0.995 0.850	6 1.000 1.000 0.997	7 1.000 1.000 0.979	8 1.000 0.984 0.772	9 1.000 1.000 1.000	10 1.000 0.975 0.769	
(mm) 6.0000 4.0000 2.0000 1.0000	1 1.000 1.000 1.000	2 1.000 0.994 0.796 0.615	3 1.000 1.000 1.000 1.000	4 1.000 1.000 1.000	5 1.000 0.995 0.850 0.679	6 1.000 1.000 0.997 0.996	7 1.000 1.000 0.979 0.940	8 1.000 0.984 0.772 0.569	9 1.000 1.000 1.000	10 1.000 0.975 0.769 0.595	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000	1 1.000 1.000 1.000 1.000 0.999	2 1.000 0.994 0.796 0.615 0.441	3 1.000 1.000 1.000 1.000 0.999	4 1.000 1.000 1.000 1.000	5 1.000 0.995 0.850 0.679 0.475	6 1.000 1.000 0.997 0.996 0.992	7 1.000 1.000 0.979 0.940 0.838	8 1.000 0.984 0.772 0.569 0.376	9 1.000 1.000 1.000 1.000	10 1.000 0.975 0.769 0.595 0.452	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500	1 1.000 1.000 1.000 1.000 0.999 0.976	2 1.000 0.994 0.796 0.615 0.441 0.283	3 1.000 1.000 1.000 1.000 0.999 0.993	4 1.000 1.000 1.000 1.000 1.000 0.998	5 1.000 0.995 0.850 0.679 0.475 0.272	6 1.000 1.000 0.997 0.996 0.992 0.965	7 1.000 1.000 0.979 0.940 0.838 0.622	8 1.000 0.984 0.772 0.569 0.376 0.213	9 1.000 1.000 1.000 1.000 1.000	10 1.000 0.975 0.769 0.595 0.452 0.343	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109	3 1,000 1,000 1,000 1,000 0,999 0,993 0,918 0,848	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716	4 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.183	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160	1 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.084	3 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585 0.489	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.183 0.134	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.040	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.084 0.070	3 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618	4 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585 0.489 0.423	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.183 0.134 0.109	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164 0.144	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.040 0.032 0.027	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560 0.491	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115 0.090	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160 0.0120 0.0080	1 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471 0.413	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.084 0.070 0.060	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618 0.541	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585 0.489 0.423 0.335	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051 0.043	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.183 0.134 0.109	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164 0.144 0.117	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.040 0.032 0.027	9 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560 0.491	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115 0.090 0.074	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160 0.0120 0.0080 0.0060	1 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471 0.413 0.336 0.287	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.084 0.070 0.060 0.048	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618 0.541 0.433	4 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585 0.489 0.423 0.335 0.282	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051 0.043 0.031	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.134 0.109 0.081	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164 0.144 0.117	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.047 0.040 0.032 0.027 0.020	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560 0.491 0.400	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115 0.090 0.074 0.056	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160 0.0120 0.0080 0.0060	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471 0.413 0.336 0.287	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.094 0.070 0.060 0.048 0.040	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618 0.541 0.433 0.366 0.283	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.657 0.489 0.423 0.335 0.282	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051 0.043 0.031 0.025	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.183 0.134 0.109 0.081 0.067	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164 0.144 0.117 0.100	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.040 0.032 0.027 0.020 0.016	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560 0.491 0.400 0.343 0.270	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115 0.090 0.074 0.056 0.046	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160 0.0120 0.0080 0.0060 0.0040	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471 0.413 0.336 0.287 0.226 0.189	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.084 0.070 0.060 0.048 0.040	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618 0.541 0.433 0.366 0.283 0.233	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585 0.489 0.423 0.335 0.282 0.214 0.171	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051 0.043 0.031 0.025 0.018	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.134 0.109 0.081 0.067 0.051	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164 0.144 0.117 0.100 0.079	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.040 0.032 0.027 0.020 0.016 0.012	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560 0.491 0.400 0.343 0.270	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115 0.090 0.074 0.056 0.046 0.034 0.028	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160 0.0120 0.0080 0.0060 0.0040 0.0030	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471 0.413 0.336 0.287 0.226 0.189	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.084 0.070 0.060 0.048 0.040 0.031 0.024	3 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618 0.541 0.433 0.366 0.283 0.233 0.177	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585 0.423 0.335 0.282 0.214 0.171 0.122	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051 0.043 0.025 0.018 0.014	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.183 0.134 0.109 0.081 0.067 0.051	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164 0.144 0.117 0.100 0.079 0.066	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.040 0.032 0.027 0.020 0.016 0.012 0.009	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560 0.491 0.343 0.270 0.226 0.173	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115 0.090 0.074 0.056 0.046 0.034 0.028	
(mm) 6.0000 4.0000 2.0000 1.0000 0.5000 0.2500 0.0740 0.0480 0.0320 0.0240 0.0160 0.0120 0.0080 0.0060 0.0040	1 1.000 1.000 1.000 1.000 0.999 0.976 0.836 0.717 0.622 0.557 0.471 0.413 0.336 0.287 0.226 0.189	2 1.000 0.994 0.796 0.615 0.441 0.283 0.127 0.109 0.094 0.084 0.070 0.060 0.048 0.040	3 1.000 1.000 1.000 1.000 0.999 0.993 0.918 0.848 0.778 0.716 0.618 0.541 0.433 0.366 0.283 0.233	4 1.000 1.000 1.000 1.000 1.000 0.998 0.891 0.759 0.657 0.585 0.489 0.423 0.335 0.282 0.214 0.171	5 1.000 0.995 0.850 0.679 0.475 0.272 0.098 0.084 0.072 0.064 0.051 0.043 0.031 0.025 0.018	6 1.000 1.000 0.997 0.996 0.992 0.965 0.688 0.387 0.238 0.134 0.109 0.081 0.067 0.051	7 1.000 1.000 0.979 0.940 0.838 0.622 0.329 0.258 0.217 0.193 0.164 0.144 0.117 0.100 0.079	8 1.000 0.984 0.772 0.569 0.376 0.213 0.081 0.058 0.047 0.040 0.032 0.027 0.020 0.016 0.012	9 1.000 1.000 1.000 1.000 1.000 1.000 0.991 0.842 0.736 0.661 0.560 0.491 0.400 0.343 0.270	10 1.000 0.975 0.769 0.595 0.452 0.343 0.214 0.174 0.136 0.115 0.090 0.074 0.056 0.046 0.034 0.028	

CURVAS GRANULOMÉTRICAS DOS PRODUTOS RESULTANTES DA 2ª AMOSTRAGEM



Run 1 of 1 Dia 05/05

File name:

Group ID:

Sample ID: Operator:

Amostra nº 1

Run number: 4

Comments:

Start time:

12:16 25 Nov 1994

Pump Speed: 75 Obscuration:

11%

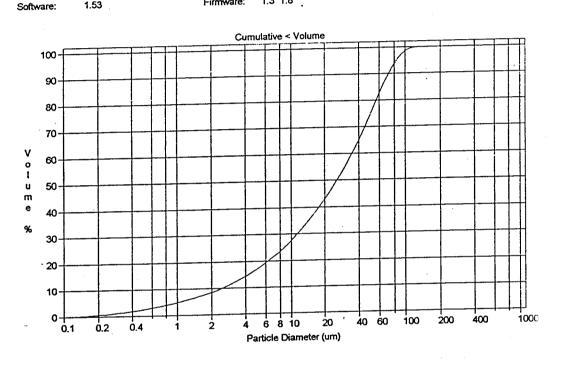
Run length: 60 Seconds

Optical model: Fraunhofer LS 130

Fluid module

1.53

Firmware: 1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume Mean: Median: 100.0% 32.09 um 25.71 um

95% Conf. Limits: 0-85 um 27 um \$.D.:

Variance: C.V.:

 $728\,\mathrm{um}^2$

Mode:

Mean/Median Ratio: 1.248 56.00 um

84.1%

Skewness: Kurtosis:

0.805 Right skewed

-0.125 Platykurtic

% < 10 Size um 2.465 8.708

50 25.71

75 50.50

Run 1 of 1 Dia 05/05

File name:

Sample ID:

Group ID:

Run number: 3

Amostra nº 2

Operator:

Comments:

Start time:

Pump Speed:

Obscuration: Optical model: Fraunhofer

LS 130

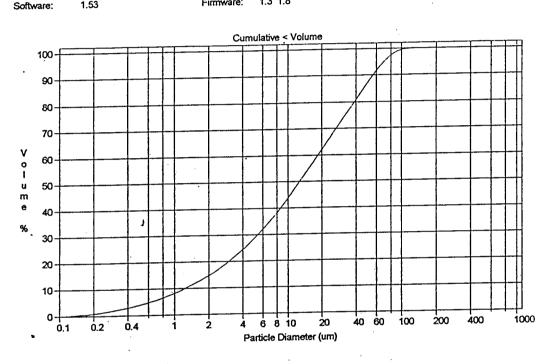
75 11% Fluid module

1.53

12:01 25 Nov 1994

Firmware: 1.3 1.8

Run length: 60 Seconds



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume . Mean:

100.0%

21.37 um

95% Conf. Limits: 0-65.6 um

12.69 um Median:

S.D.:

22.6 um

Mean/Median Ratio: 1.684

Variance:

 $509 \, \text{um}^2$

Mode:

35.52 um

C.V.:

106%

Skewness: Kurtosis:

1.4 Right skewed 1.46 Leptokurtic

10

4.123 Size um 1.240

50 12.69

32.20

11:46 25 Nov 19

Run 1 of 1

File name:

Sample ID:

Amostra nº 3

Group ID:

Dia 05/05

Operator:

Comments: Start time:

Run number: 2

11:44 25 Nov 1994

Run length: 60 Seconds

Pump Speed: Obscuration: Optical model:

75 16%

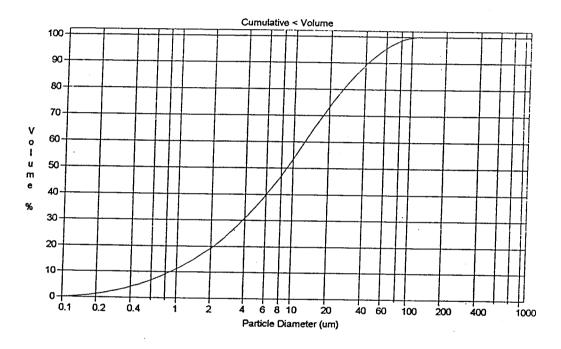
Fraunhofer Fluid module

LS 130 Software:

1.53

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean:

15.87 um

Median:

8.879 um

95% Conf. Limits: S.D.:

0-52.8 um 18.8 um

Mean/Median Ratio: 1.787

Variance:

354 um²

Mode: 11.91 um

C.V.:

Skewness:

119%

Kurtosis:

1.97 Right skewed 4.17 Leptokurtic

% < 10 Size um 0.881

25 2.931 50 8.879 75 21.34

15:23 13 Jan 199

Run 1 of 1

File name:

Group ID: 5/5/94

Sample ID:

Operator: Comments:

Run number: 3

Start time: Pump Speed:

100

15:21 13 Jan 1995

Run length: 61 Seconds

Obscuration:

LS 130

Software:

12%

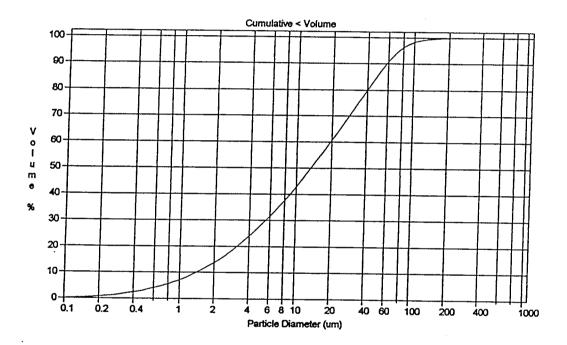
4

Optical model: Fraunhofer

Fluid module

1.53

Firmware: 1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean: Median:

22.95 um

13.27 um

S.D.:

95% Conf. Limits: 0-74.2 um 26.1 um

682 um²

Mean/Median Ratio: 1.729 Mode:

35.52 um

Variance: C.V.:

Skewness:

114%

Kurtosis:

2.13 Right skewed 6.83 Leptokurtic

10 Size um 1.406

25 4.242 50 13.27

33.52

OULTERR LS Particle Size Analysis

11:31 28 Nov 1994

Run 1 of 1

File name:

Dia 05/05 Group ID:

Sample ID:

Operator:

Amostra nº 5

Run number: 2

Comments: Start time:

.s 130

ioftware:

11:29 28 Nov 1994

²ump Speed: 75 11%

Run length: 60 Seconds

Obscuration:

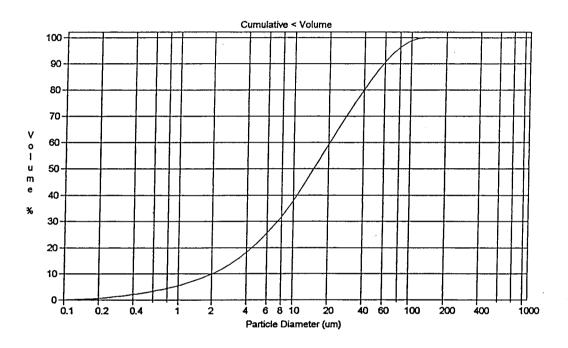
Optical model: Fraunhofer

Fluid module

1.53

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

ilculations from 0.100 um to 900.0 um

lume

100.0%

an:

23.38 um

xdian: 14.87 um

S.D.:

95% Conf. Limits: 0-69.8 um

Variance:

23.7 um 562 um²

san/Median Ratio: 1,572 xde:

15.65 um

C.V.:

Skewness:

101%

Kurtosis:

1.52 Right skewed

2.13 Leptokurtic

% < 10 Size um 2,008

25 5.844

50 14.87

75 33.58

11:45 28 Nov 1994

Run 1 of 1

File name:

Sample ID:

Amostra nº 6

Dia 05/05 Group ID:

Run length: 60 Seconds

Operator:

Comments:

11:43 28 Nov 1994

Run number: 3

Start time:

Pump Speed: 75 Obscuration:

11% Fraunhofer

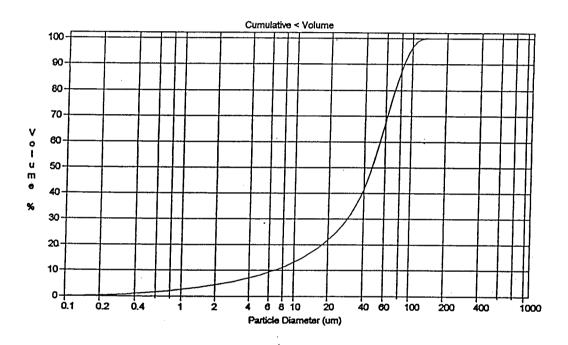
Optical model: LS 130

Fluid module

Software:

1.53

Firmware: 1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

/olume Yean:

100.0%

Mode:

vledian:

46.47 um 46.44 um

Vean/Median Ratio: 1.001 61.34 um 95% Conf. Limits: 0-102 um S.D.:

28.5 um

Variance:

810 um²

C.V.: Skewness: 61.2%

Kurtosis:

0.232 Right skewed -0.604 Platykurtic

% < 10

Size um 6.730

25 23.65 50 46.44

75 66.59

15:09 13 Jan 19

Run 1 of 1

File name: Sample ID:

Group (D: 5/5/94

Operator:

Run number: 2

Comments: Start time:

repetida

15:07 13 Jan 1995 100

Run length: 60 Seconds

1.3 1.8

Pump Speed: Obscuration:

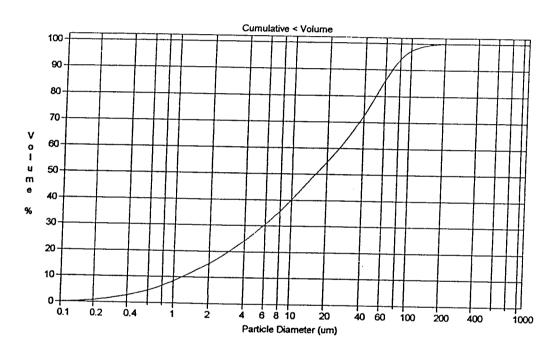
13%

Optical model: Fraunhofer

LS 130 Software:

1.53

Fluid module Firmware:



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean: Median:

27.35 um 16.02 um

95% Conf. Limits: S.D.:

0-85.6 um 29.7 um

Mean/Median Ratio: 1.707 Mode:

51.13 um

Variance: C.V.:

884 um² 109%

Skewness:

1.62 Right skewed

Kurtosis:

3.27 Leptokurtic

10 Size um 1.190

4.234

50 16.02

75 43.08

Run 1 of 1 Dia 05/05

File name:

Sample ID:

Amostra nº 8

Operator:

Comments:

Start time:

Pump Speed: 75 11%

Obscuration: Optical model: Fraunhofer LS 130

Software:

Fluid module 1.53

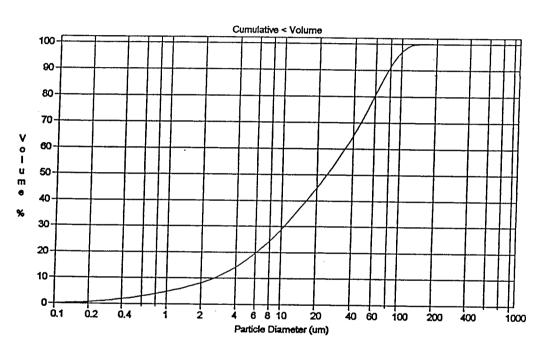
11:59 28 Nov 1994

Group ID:

Run number: 4

Run length: 61 Seconds

Firmware: 1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean: Median:

33.06 um 24.22 um

95% Conf. Limits: 0-90.9 um S.D.:

29.5 um

Mean/Median Ratio: 1.365 Mode: 61.34 um

Variance:

871 um²

C.V.:

89.3%

Skewness:

0.952 Right skewed

Kurtosis:

0.179 Leptokurtic

% < 10 Size um 2.593

25 8.258

50 24.22

52.37

11:41 11 Jan 199

Run 1 of 1

File name: 9

Group ID:

Sample ID: Operator: Comments:

Run number: 2

Start time:

11:39: 11 Jan 1995

Run length: 61 Seconds

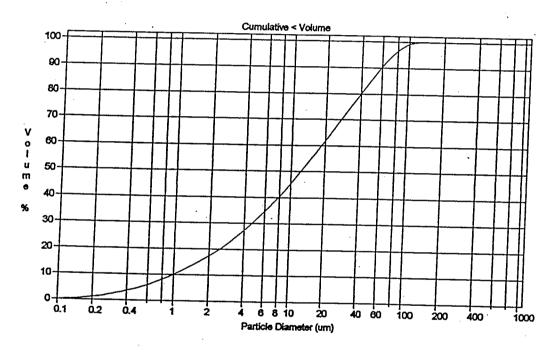
Pump Speed: 75 Obscuration: 12%

Software:

Optical model: Fraunhofer LS 130 Fluid modul

Fluid module 1.53

Firmware: 1.3 1.8



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean: Median:

21.84 um

12.24 um

S.D.:

95% Conf. Limits: 0-69 um

24.1 um

Mean/Median Ratio: 1.785

32.43 um

Variance:

580 um²

C.V.: Skewness: 110%

Kurtosis:

1.43 Right skewed

1.54 Leptokurtic

% < 10 25 3.481

50 12.24

75

90

Size um 0.988

32.95

Run 1 of 1 lab IGM

File name:

Group ID:

Sample ID: Operator:

amostra 10

Comments: Start time:

15:45 28 Dec 1994

Pump Speed: 75

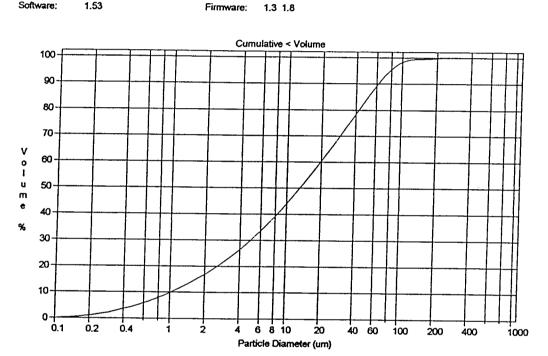
15% Obscuration: Optical model: Fraunhofer

LS 130 Software: Fluid module 1.53

Run number: 4

Run length: 61 Seconds

Firmware:



Volume Statistics (Arithmetic)

(Untitled)

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Mean: Median: 23.71 um 12.98 um

95% Conf. Limits: 0-78.9 um S.D.:

28.1 um

Mean/Median Ratio: 1.826 Mode:

Variance:

792 um²

38.91 um

C.V.:

119%

Skewness:

75

35.17

2.34 Right skewed

Kurtosis:

9.29 Leptokurtic

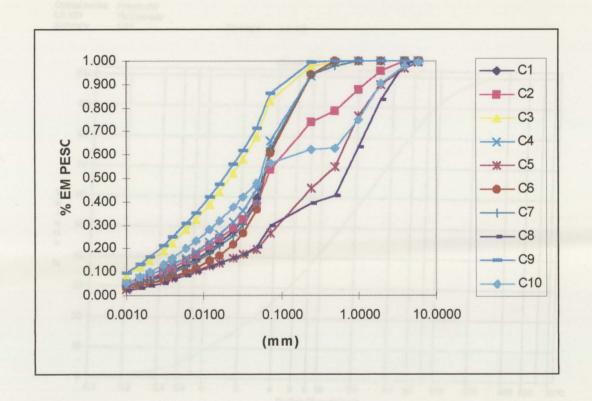
% < 10 Size um 1.023 25 3.661

50 12.98

AMOSTRAGEM N°3

Section of the Control	HISTOGRAMA							ter animana		
(mm)	C1	C2	C3	C4	C5	C6	C7	C8	C9	C10
6.0000	0.000	0.000	0.000	0.000	0.027	0.000	0.000	0.006	0.000	0.021
4.0000	0.000	0.040	0.000	0.000	0.069	0.000	0.000	0.157	0.000	0.072
2.0000	0.000	0.082	0.000	0.000	0.135	0.000	0.000	0.201	0.000	0.157
1.0000	0.005	0.088	0.003	0.008	0.215	0.001	0.019	0.207	0.000	0.123
0.5000	0.056	0.048	0.016	0.059	0.095	0.060	0.037	0.033	0.006	0.004
0.2500	0.322	0.205	0.150	0.277	0.192	0.334	0.314	0.093	0.133	0.058
0.0740	0.205	0.145	0.154	0.202	0.065	0.236	0.235	0.092	0.147	0.083
0.0480	0.090	0.066	0.094	0.094	0.025	0.105	0.092	0.031	0.094	0.060
0.0320	0.049	0.037	0.061	0.049	0.015	0.047	0.044	0.018	0.063	0.042
0.0240	0.053	0.045	0.079	0.053	0.020	0.045	0.047	0.023	0.081	0.056
0.0160	0.030	0.030	0.052	0.032	0.013	0.025	0.029	0.016	0.053	0.038
0.0120	0.036	0.039	0.069	0.040	0.019	0.029	0.036	0.021	0.070	0.052
0.0080	0.021	0.024	0.043	0.024	0.013	0.016	0.022	0.014	0.044	0.032
0.0060	0.026	0.030	0.054	0.031	0.017	0.020	0.026	0.018	0.058	0.041
0.0040	0.016	0.019	0.034	0.019	0.011	0.012	0.016	0.012	0.037	0.026
0.0030	0.020	0.023	0.043	0.024	0.014	0.015	0.019	0.015	0.047	0.032
0.0020	0.013	0.015	0.028	0.016	0.010	0.010	0.011	0.009	0.032	0.020
0.0015	0.017	0.019	0.036	0.021	0.013	0.012	0.015	0.011	0.039	0.026
0.0010	0.042	0.043	0.085	0.051	0.029	0.033	0.037	0.021	0.096	0.055
SUM	1.000	0.998	1.000	1.000	0.996	1,000	0.999	0.998	1.000	0.997
<u> Principal</u>		W. 5.357 W			LYVENS	ERLER .				
(mm)	C1	C2	C3	C4	C5	C6	C7	C8	C9	C10
6.0000	1.000	0.998	1.000	1.000	0.996	1.000	0.999	0.998	1.000	0.997
4.0000	1.000	0.998	1.000	1.000	0.970	1.000	0.999	0.992	1.000	0.977
2.0000	1.000	0.958	1.000	1.000	0.901	1.000	0.999	0.834	1.000	0.905
1.0000	1.000	0.876	1.000	1.000	0.765	1.000	0.999	0.633	1.000	0.748
0.5000	0.995	0.788	0.997	0.992	0.550	0.999	0.980	0.426	1.000	0.625
0.2500	0.939	0.740	0.981	0.934	0.455	0.939	0.943	0.393	0.994	0.621
0.0740	0.618	0.535	0.831	0.657	0.264	0.605	0.629	0.300	0.861	0.563
0.0480	0.413	0.391	0.676	0.455	0.198	0.369	0.394	0.208	0.714	0.479
0.0320	0.323	0.325	0.582	0.361	0.173	0.264	0.301	0.177	0.619	0.419
0.0240	0.274	0.288	0.522	0.312	0.158_	0.217	0.258	0.159	0.556	0.378
0.0160	0.221	0.242	0.443	0.259	0.139	0.171	0.210	0.136	0.475	0.322
0.0120	0.191	0.213	0.391	0.227	0.125	0.147	0.182	0.121	0.422	0.283
0.0080	0.155	0.174	0.322	0.187	0.106	0.118	0.145	0.099	0.352	0.232
0.0060	0.134	0.150	0.280	0.162	0.094	0.102	0.124	0.085	0.308	0.200
0.0040	0.108	0.119	0.226	0.132	0.077	0.082	0.097	0.067	0.250	0.159
0.0030	0.092	0.100	0.191	0.112	0.066	0.070	0.082	0.056	0.213	0.133
0.0020	0.072	0.077	0.149	0.088	0.051	0.055	0.063	0.041	0.166	0.101
0.0015	0.059	0.062	0.121	0.072	0.042	0.045	0.051	0.032	0.135	0.080
0.0010	0.042	0.043	0.085	0.051	0.029	0.033	0.037	0.021	0.096	0.055

CURVAS GRANULOMÉTRICAS DOS PRODUTOS RESULTANTES DA 3ª AMOSTRAGEM



11:58 12 Dec 199

File name: FINAL.\$02

Group ID: final

Sample ID: Operator: Comments:

Run number: 2

Start time:

11:56 12 Dec 1995

75

Pump Speed: Obscuration:

10% Fraunhofer

Optical model: LS 130 Software:

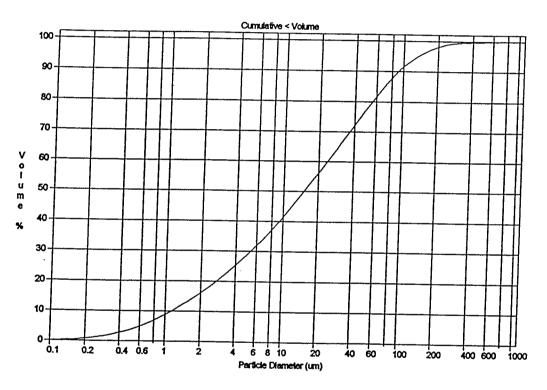
Fluid module 1.53

Firmware:

1.3 1.8

Run length: 60 Seconds

final.\$02



Volume Statistics (Arithmetic)

final.\$02

Calculations from 0.100 um to 900.0 um

Meer: Median: Mean/Median Ratio: 2.338

Volume

Mode:

100.0% 35.09 um

15.01 um 42.62 um

95% Conf. Limits: 0-142 um 8.D.:

54.8 um 3000 um²

Variance: C.V.: Skewness:

156% 4.41 Right skewed

Kurtosis: 34.4 Leptokurtic

90 90.82

% < 10 Size um 1.140 25 3.918 50 15.01 75 45.02

finel.\$03

12:15 12 Dec 199:

File name: Sample ID: FINAL \$03 n°2

Group ID:

Run number: 3

Operator:

Comments: Start time:

12:13 12 Dec 1995

Pump Speed: Obscuration:

10%

Optical model: Fraunhofer LS 130 Fluid module Software:

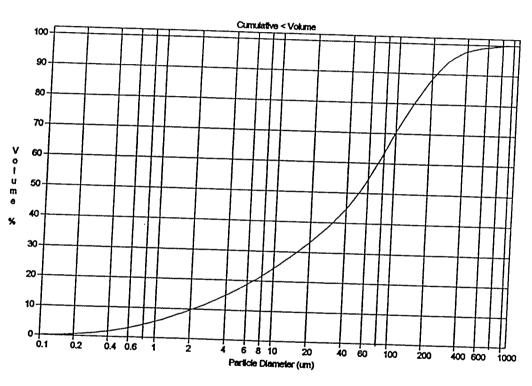
1.53

Firmware:

1.3 1.8

Run length: 60 Seconds

final



Volume Statistics (Arithmetic)

final.\$03

talculations from 0.100 um to 900.0 um

'olume

lode:

100.0%

80.61 um

loan: 86.58 um iedian

60.22 um

lean/Median Ratio: 1.724

95% Conf. Limits: 0-306 um

S.D.: Variance:

112 um

1.25e+004 um²

C.V.: Skewness:

2.72 Right skewed 10.6 Leptokurtic

Kurtosis:

%< 10 Size um 2.110

25 10.55

50 50.22

118.1

12:29 12 Dec 199

final.\$04

File name: Sample ID: final.\$04 nº3

Group ID: finel

Operator: Comments:

Run number: 4

12:26 12 Dec 1995 75

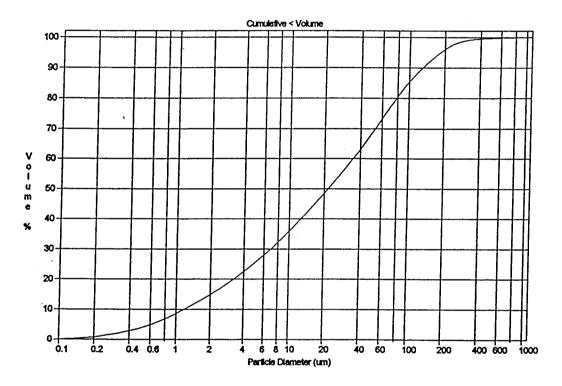
Start time: Pump Speed:

Run length: 60 Seconds

Obscuration: 10% Optical model: Fraunhofer LS 130 Fluid module

Software: 1.53

Firmwere: 1.3 1.8



Volume Statistics (Arithmetic)

final.\$04

Calculations from 0.100 um to 900.0 um

Volume 100.0%

Mean: 48.23 um

Median; 21.54 um Meen/Median Ratio: 2.240 Mode: 61.34 um 95% Conf. Limits: 0-187 um

S.D.: 70.8 um 5010 um² Varianca:

C.V.:

Skewness: Kurtosis:

147% 3.71 Right skewed 24.3 Leptokurtic

% < 10 Size um 1.192 25 4.835

50 21.54

75 64.26

final.\$05

File name: Sample ID:

FINAL.\$05

Group ID: final

Run number: 5

Operator.

Comments:

12:39 12 Dec 1995

Run length: 61 Seconds

Start time: 100 Pump Speed:

9%

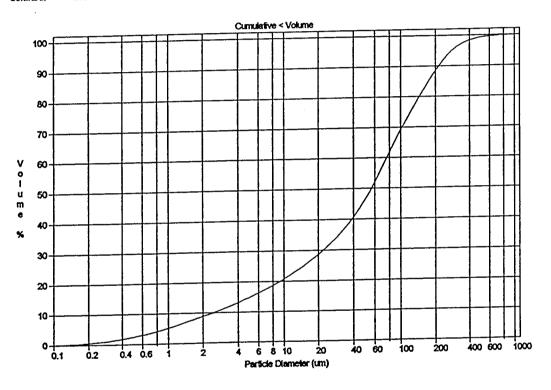
Obscuration: Fraunhofer

Optical model: LS 130 Software:

Fluid module 1.53

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

final.\$05

Calculations from 0.100 um to 900.0 um

/olume Moon: declar: 100.0% 86.81 um

95% Conf. Limits: 0-284 um S.D.:

101 um

Mean/Median Ratio: 1.550

56.01 um

Variance:

1.01e+004 um²

73.59 um lode:

C.V.:

Skewness: Kurtosis:

116% 2.42 Right skewed 9.24 Leptokuriic

% < 10 Size um 2.465

25 14.85

50 56.01

75 121.8

11:59 15 Dec 19:

final.\$11

File name:

Sample ID: Operator:

FINAL\$11 m*5

Group ID: Final

Run length: 61 Seconds

Comments:

11:57 15 Dec 1995

Run number: 5

Start time: Pump Speed: Obscuration:

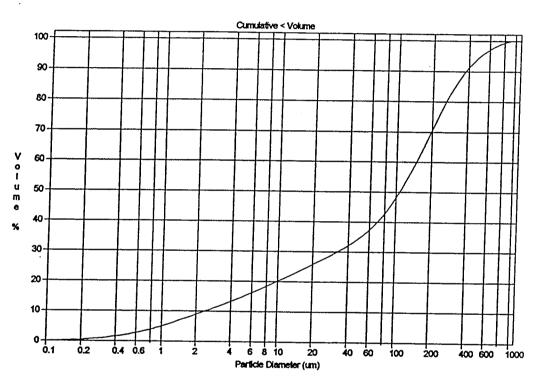
75 10% Fraunhofer Optical model: Fluid module

LS 130 Software:

1.53

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

final\$11

Calculations from 0.100 um to 900.0 um

Volume

Mean Median:

100.0% 154.1 um 107.2 um

S.D.:

95% Conf. Limits: 0-481 um

Mean/Median Ratio: 1.438 Mode: 200.4 um Variance:

167 um 2.78e+004 um²

C.V.: Skewness: 108% 1.61 Right skewed 2.79 Leptokurtic

Kurtosis:

%< 10 Size um 2.412

25 18.29

50 107.2

75 225.9

QUILTERR LS Particle Size Analysis

12:55 12 Dec 1995

final.\$06

File name: Sample ID: Operator: Comments:

FINAL \$06 n*6

Group ID:

Run number: 6

Start time:

12:53 12 Dec 1995

100 Pump Speed:

Obscuration: Optical model: LS 130

Software:

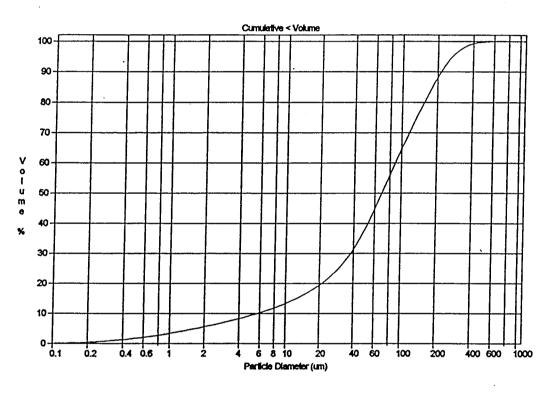
Fraunhofer Fluid module 1.53

Firmware:

1.3 1.8

final

Run length: 60 Seconds



Volume Statistics (Arithmetic)

final \$06

alculations from 0,100 um to 900.0 um

'olume

100.0%

lean: ledian:

93.10 um 68.71 um

S.D.:

95% Conf. Limits: 0-261 um

Variance:

85.9 um

lean/Median Ratio: 1.355 73.59 um

7370 um²

C.V.: Skewness:

Kurtosis:

1.46 Right skewed 2.55 Leptokurtic

10

Size um 5.791

25 29.70

60 68.71

75 134.2

11:34 15 Dec 199

final.\$09

File name: Sample ID: FINAL.\$09

Group ID:

Operator:

Run number: 3

Comments: Start time:

11:32 15 Dec 1995

Run length: 60 Seconds

Pump Speed: Obscuration

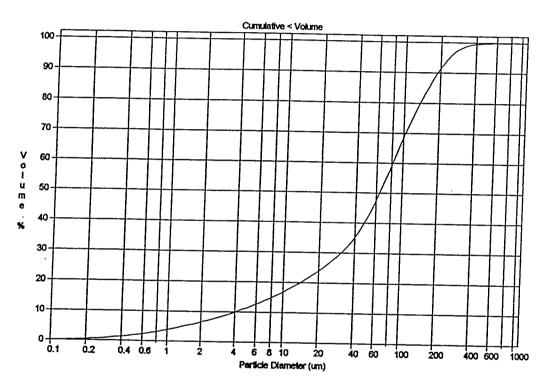
75 9% Fraunhofer

Optical model: LS 130 Software: 1.53

Fluid module

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

final.\$09

Calculations from 0.100 um to 900.0 um

Volume

100.0%

Moon:

83.15 um

S.D.:

95% Conf. Limits: 0-241 um 80.5 um

Median: 64.01 um Mean/Median Ratio: 1.299 Mode:

80.61 um

Variance: C.V.:

6480 um²

Skewness:

Kurtosis:

96.8% 2.05 Right skewed 8.92 Leptokurtic

% < 10 Size um 4.059

25 21.81

50 64.01

75 118.8

COULTERR LS Particle Size Analysis

final.\$08

ile name: Sample ID:

FINAL \$08

nº 8

Group ID: Final Run number: 2

Run length: 61 Seconds

Operator.

Comments: 11:19 15 Dec 1995

Start time:

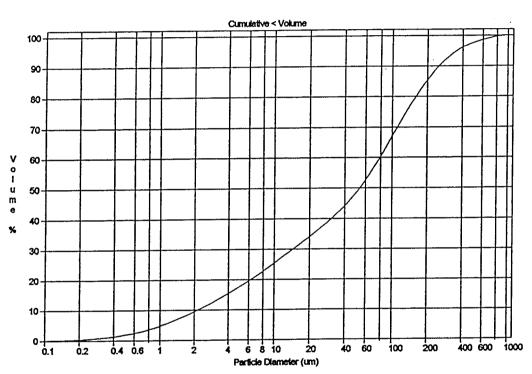
75 10% 'ump Speed: Obscuration:
Optical model:
S 130 Fraunhofer

ioftware:

1.53

Fluid module

1.3 1.8 Firmware:



Volume Statistics (Arithmetic)

final.\$08

alculations from 0.100 um to 900.0 um

okume eart:

100.0% 98.01 um

eclano 53.43 um

ean/Median Ratio: 1.834 96.71 um ode:

Variance:

95% Conf. Limits: 0-353 um 130 um S.D.:

1.69e+004 um² 133%

C.V.: Skewness:

2.52 Right skewed

Kurtosis:

8.11 Leptokurlic

50 75 53.43 132.8 90 249.2 %< 10 Size um 2.161 25 9.689

File name:

· FINAL.\$07

Group ID: Final

Sample ID: Operator:

n* 9

Comments:

11:03 15 Dec 1995

Run number: 1 Run length: 60 Seconds

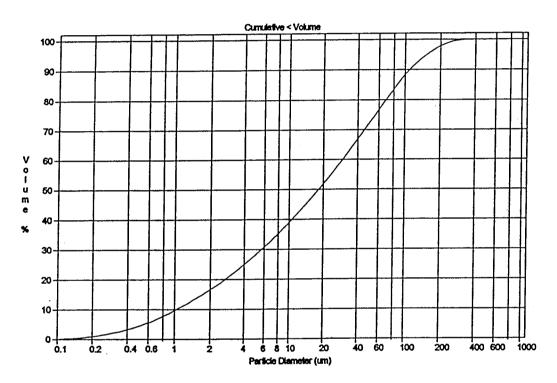
Start time: Pump Speed: Obscuration:

75 10% Optical model: Fraunhofer LS 130 Fluid module

Fluid module

1.53 Software:

Firmwere: 1.3 1.8



Volume Statistics (Artifrmetic)

final.\$07

Calculations from 0.100 um to 900.0 um

Volume Mean: Median: 100.0%

39.75 um 18.24 um

95% Conf. Limits: 0-142 um S.D.: 0-142 um

Mean/Median Ratio: 2.180 Mode: 56.001 56.00 um

Variance: C.V.:

2700 um² 131%

2.05 Right skewed Skewness: 4.69 Leptokurtic Kurtosis:

% < 10 Size um 1.049 25 4.002 50 18.24 75 55.94 90 109.8 COULTER^R LS Particle Size Analysis

11:46 15 Dec 1995

final.\$10

File name:

FINAL.\$10 nº 10

Group ID: Final

Run length: 60 Seconds

Sample ID: Operator:

Run number: 4

Comments: Start time:

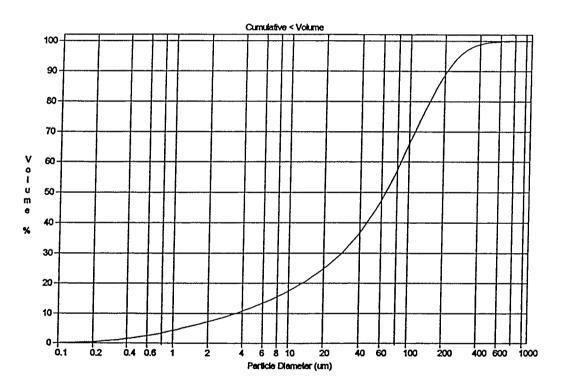
11:44 15 Dec 1995 75 10%

Pump Speed: Obscuration: Optical model: Fraunhofer

LS 130 Software: Fluid module 1.53

Firmware:

1.3 1.8



Volume Statistics (Arithmetic)

finel.\$10

Calculations from 0.100 um to 900.0 um

/olume lean:

100.0%

fedian:

89.80 um 64.73 um

AeeryMedian Ratio: 1.387

95% Conf. Limits: 0-271 um S.D.:

92.6 um

fode: 96.71 um 8570 um²

Variance: C.V.: Skewness:

Kurtosis:

103% 2 Right skewed 6.72 Leptokurtic

% < 10 Size um 3.502

25 20.24

50 64.73

75 129.2

90 209.0

PERCENTAGEM DE SÓLIDOS E DILUIÇÃO

PERCENTAGEM DE SÓLIDOS E DILUIÇÃO PARA AS TRÊS AMOSTRAGENS REALIZADAS

	Amostra	igem N°1	Amostag	em N°2	· Amosira	igem N°3
	P _s %	D	P _s %	D	Ps %	D
N°1	33.7	1.967	32.5	2.077	34.0	1.941
N' 2	70.5	0.418	72.5	0.379	71.5	0.399
AY3	30.0	2.333	30.6	2.266	34.7	2.155
Nº4	32.7	2.058	31.9	2.135	38.3	1.611
S _N S	83.1	0.203	82.2	0.217	78.9	0.267
: Nº6	46.1	1.169	45.6	1.198	42.8	1.232
Nº7	49.3	1.028	60.5	0.653	55.1	0.957
Nº8	83.4	0.199	82.4	0.214	83.2	0.202
1,10	24.3	3.115	26.8	2.731	25.6	2.759
Nº10	70.0	0.429	65.6	0.524	78.6	0.397

ANEXO II

ESTIMA DOS CAUDAIS MÁSSICOS RESULTADOS DE VÁRIAS HIPÓTESES

- AMOSTRAGEM 1
- HIPÓTESE DE ABANDONO DO FLUXO 4.
- HIPÓTESE DE ABANDONO DO FLUXO 7.
- HIPÓTESE DE ABANDONO DO FLUXO 8.
- AMOSTRAGEM 2
- HIPÓTESE DE ABANDONO DO FLUXO 1.
- AMOSTRAGEM 3
- HIPÓTESE DE ABANDONO DO FLUXO 1.

RESULTADOS DO CÁLCULO DOS CAUDAIS MÁSSICOS RESULTANTES DA HIPÓTESE DO ABANDONO DO FLUXO 4

1 μ	1.5 μ	2μ	3 μ	4μ	6 μ	8 μ	12 μ	16 µ	24 μ	32 µ	48 µ	74 µ
-0.95	-1.62	-7.03	0.89	0.27	-0.01	-0.09	-0.14	-0.15	-0.16	-0.15	-0.14	-0.11
-0.06	0.82	8.02	-2.61	-1.78	-1.36	-1.19	-0.99	-0.89	-0.79	-0.73	-0.65	-0.56
-0.88	-2.44	-15.06	3.50	2.06	1.36	1.10	0.85	0.74	0.63	0.57	0.51	0.45
-0.02	0.34	3.67	-1.33	-0.94	-0.70	-0.58	-0.43	-0.34	-0.24	-0.19	-0.12	-0.04
-0.04	0.48	4.35	-1.28	-0.85	-0.66	-0.60	-0.57	-0.56	-0.54	-0.54	-0.53	-0.52
-0.99	-2.55	-15.17	3.39	1.95	1.25	1.00	0.75	0.64	0.52	0.46	0.39	0.32
-1.90	-3.11	-12.38	1.17	0.12	-0.35	-0.48	-0.57	-0.60	-0.61	-0.62	-0.61	-0.59
0.89	0.89	0.89	0.89	0.89	0.90	0.90	0.90	0.90	0.89	0.89	0.88	0.87
0.11	0.11	0.11	0.11	0.11	0.10	0.10	0.10	0.10	0.11	0.11	0.12	0.13

RESULTADOS DO CÁLCULO DOS CAUDAIS MÁSSICOS RESULTANTES DA HIPÓTESE DO ABANDONO DO FLUXO 7

1μ	1.5 μ	2μ	3 μ	4 μ	6 μ	8 µ	12 µ	16 µ	24 μ	32 µ	48 µ	74 µ
0.19	0.19	0.19	0.18	0.18	0.18	0.17	0.17	0.17	0.17	0.17	0.17	0.08
0.01	0.02	0.02	0.02	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.02	0.00
0.17	0.17	0.17	0.16	0.16	0.15	0.14	0.14	0.14	0.14	0.14	0.14	0.08
2.21	2.15	2.11	2.08	2.11	2.25	2.45	3.12	4.25	10.57	-52.63	-4.14	-1.27
-2.20	-2.13	-2.09	-2.06	-2.08	-2.22	-2.42	-3.09	-4.22	-10.54	52.66	4.17	1.28
0.06	0.06	0.06	0.05	0.05	0.04	0.04	0.04	0.04	0.03	0.03	0.02	-0.06
1.39	1.32	1.28	1.24	1.27	1.39	1.60	2.26	3.39	9.71	-53.49	-5.00	-2.20
0.89	0.89	0.89	0.89	0.89	0.90	0.90	0.90	0.90	0.89	0.89	0.88	0.87
0.11	0.11	0.11	0.11	0.11	0.10	0.10	0.10	0.10	0.11	0.11	0.12	0.13

RESULTADOS DO CÁLCULO DOS CAUDAIS MÁSSICOS RESULTANTES DA HIPÓTESE DO ABANDONO DO FLUXO 8

1μ	1.5 µ	2μ	3 μ	4 μ	6 µ	8 µ	12 μ	16 µ	24 μ	32 µ	48 µ	74 µ
-1.32	-1.33	-1.33	-1.34	-1.34	-1.33	-1.32	-1.32	-1.31	-1.28	-1.27	-1.28	-1.24
-0.09	-0.11	-0.13	-0.16	-0.18	-0.21	-0.22	-0.23	-0.24	-0.23	-0.22	-0.18	-0.06
-1.23	-1.22	-1.20	-1.17	-1.15	-1.12	-1.10	-1.09	-1.07	-1.05	-1.05	-1.10	-1.18
-0.39	-0.39	-0.39	-0.39	-0.38	-0.36	-0.35	-0.33	-0.31	-0.29	-0.28	-0.26	-0.23
0.30	0.28	0.27	0.23	0.20	0.16	0.13	0.09	0.07	0.06	0.06	0.08	0.17
0.03	0.04	0.05	0.07	0.09	0.10	0.11	0.13	0.14	0.17	0.21	0.28	0.44
-2.61	-2.61	-2.60	-2.56	-2.53	-2.49	-2.46	-2.41	-2.38	-2.34	-2.33	-2.36	-2.41
2.26	2.26	2.25	2.25	2.24	2.23	2.22	2.21	2.21	2.22	2.26	2.38	2.62
-1.26	-1.26	-1.25	-1.25	-1.24	-1.23	-1.22	-1.21	-1.21	-1.22	-1.26	-1.38	-1.62

AMOSTRAGEM N°2

				CAL	CULO DOS	AUDAIS DO	S DADOS DA	2ª AMOSTRA	GEM				
	74 µ	48 µ	32 μ	24 µ	16 µ	12 µ	8 µ	¢р	4 µ	3 р	2 μ	1.6 p	1 µ
Q1	0.652	0.432	2.337	1.242	1.238	1.229	1.219	1.217	1.210	1.191	1.170	1.153	1.129
Q2	0.563	0.278	1.714	1.053	1.108	1.122	1.123	1.125	1.122	1.104	1.084	1.070	1.051
Q3.	0.089	0.154	0.622	0.189	0.130	0.107	0.096	0.091	0.089	0.087	0.086	0.084	0.078
Q4	0.020	0.010	0.047	0.017	0.011	0.020	0.033	0.047	0.060	0.071	0.078	0.080	0.067
Q5	0.543	0.268	1.667	1.037	1.097	1.102	1.090	1.079	1.062	1.033	1.006	0.990	0.984
Q6	-0.047	-0.125	0.405	0.010	-0.025	-0.028	-0.023	-0.017	-0.012	-0.007	-0.003	-0.001	-0.003
07	-0.368	-0.578	1.289	0.225	0.227	0.209	0.186	0.170	0.150	0.121	0.092	0.073	0.062
Q8	0.864	0.721	0.783	0.821	0.845	0.865	0.881	0.892	0.900	0.906	0.911	0.915	0.919
Q9	0.136	0.279	0.217	0.179	0.155	0.135	0.119	0.108	0.100	0.094	0.089	0.085	0.081
Q10	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000

			CALCULO DO	S CAUDAIS	DOS DADOS	DA 2ª AMOST	RAGEM CO	VI CUMULANT	E		
	48 µ	32 p	24 μ	16 µ	. 48	¢ρ	4.μ	3 µ	2 µ	1.6 µ	1 p
Q1 :::	1.159	1.181	1.190	1.190	1.185	1.177	1.171	1.162	1.154	1.143	1.137
Q2	1.014	1.061	1.083	1.094	1.093	1.089	1.086	1.078	1.072	1.063	1.057
Q3	0.145	0.119	0.107	0.096	0.091	0.087	0.085	0.083	0.082	0.081	0.080
Q4	0.037	0.039	0.041	0.046	0.051	0.059	0.064	0.069	0.072	0.073	0.071
Q5	0.976	1.022	1.042	1.048	1.042	1.030	1.022	1.009	1.000	0.990	0.986
Q6	-0.002	-0.010	-0.012	-0.013	-0.012	-0.009	-0.007	-0.005	-0.004	-0.003	-0.002
Q7	0.122	0.142	0.149	0.144	0.133	0.117	0.107	0.092	0.082	0.071	0.066
Q8	0.852	0.871	0.880	0.891	0.897	0.904	0.908	0.912	0.914	0.917	0.918
Qs	0.148	0.129	0.120	0.109	0.103	0.096	0.092	0.088	0.086	0.083	0.082
Q10	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000

AMOSTRAGEM N°3

					CÁLC	ULO DE C	AUDAIS C/	HISTOGR!	AMA 3° AM	OSTRAGE	VI.				
	600 µ	260 µ	74 µ	48 µ	32 µ	24 µ	16 p	12 µ	8 µ	6 р	4 µ	3 μ	2 µ	1.5 g	1 µ
Q1	1.65	3.01	2.14	1.64	1.95	2.22	3.22	7.72	7.72	11.23	6.43	4.76	3.72	4.33	3.50
Q2	0.32	3.94	2.31	1.19	1.32	1.61	2.60	7.08	7.08	10.58	5.80	4.14	3.11	3.74	2.95
03	1.33	-0.94	-0.17	0.44	0.63	0.61	0.62	0.64	0.64	0.64	0.63	0.62	0.61	0.59	0.55
Q4	0.41	0.60	1.34	0.70	0.88	1.23	2.26	6.77	6.77	10.26	5.48	3.77	2.54	2.85	1.91
Q6	-0.09	3.34	0.97	0.49	0.44	0.38	0.33	0.32	0.32	0.32	0.32	0.37	0.57	0.89	1.04
QG	0.24	-0.08	-0.01	-0.02	0.11	0.04	0.02	0.02	0.02	0.04	0.07	0.08	0.11	0.07	
Q7	0.24	1.40	-0.20	-0.07	0.07	-0.01	-0.04	-0.04	-0.04	-0.03	-0.05	-0.01	-0.18	-0.48	0.09
Q8	-0.09	1.85	1.16	0.54	0.48	0.44	0.39	0.38	0.38	0.39	0.44	0.46	0.50		-0.59
Q9	1.09	-0.85	-0.16	0.46	0.52	0.56	0.61	0.62	0.62	0.61	0.56	0.54		0.48	0.54
Q10	1.00	0.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1,00	1.00

11111111111													
				CALCU	LO DE CAL	IDAIS C/ C	UMULANT	E 3º AMOS	TRAGEM				
	260 μ	74 p	48 µ	32 p	24 µ	16 µ	8 µ	60	4.μ	3 μ	2 µ	1.6 µ	(p
Q1	5.62	6.28	9.01	13.84	18.73	25.68	28.85	29.87	30.61	32.88	36.22	42.06	47.00
Q2	8.09	8.40	11.14	16.17	21.27	28.59	32.09	33.71	34.95	38.10	42.25	49.55	55.96
Q3	-2.46	-2.12	-2.12	-2.34	-2.54	-2.91	-3.25	-3.84	-4.34	-5.22	-6.02	-7.49	-8.96
Q4	4.81	5.80	8.36	13.11	17.91	24.70	27.68	28.25	28.50	29.58	31.50	34.74	37.94
Q5	3.27	2.60	2.78	3.06	3.36	3.89	4.41	5.46	6.44	8.52	10.75	14,81	18.03
Q6	-0.56	-0.25	-0.23	-0.24	-0.26	-0.30	-0.37	-0.49	-0.59	-0.76	-0.92	-1.20	-1.39
Q7	-0.19	-0.52	-0.35	-0.27	-0.18	-0.02	0.17	0.62	1.11	2.30	3.72	6.32	8.06
Q8	2.90	2.87	2.89	3.09	3.29	3.61	3.88	4.35	4.75	5.46	6.10	7.29	8.57
Q9	-1.90	-1.87	-1.89	-2.09	-2.29	-2.61	-2.88	-3.35	-3.75	-4.46	-5.10	-6.29	-7.57
Q10	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00

ANEXO III

PROGRAMAS EM PASCAL

- -PROGRAMA CICLONE AJUSTA MODELOS DE CURVAS DE PARTIÇÃO
- -PROGRAMA A.P.C.V.1 SIMULADOR C/ VARIAÇÃO DE As E D50 COM O RENDIMENTO PONDERAL.
- -PROGRAMA A.P.C.V.2 SIMULADOR C/ As E D50 FIXOS

PROGRAM CICLONE(INPUT,OUTPUT,RESULT);

```
USES wincrt;
 LABEL 10,20,30,40,50,60;
 TYPE VECTOR = Array [1..20] of Extended;
    PARAM = Array [1..4] of Extended;
    RESIDUO = Array [1..20] of Extended;
 VAR i,j,k,n,op,KK,IJ,IX,JX,JK,MAXE,MO,M,NE,NN,NP,FLAG:integer;
    m1.Pi.Corte.R.U.AM.Infra.Soma.DOWN.KOUNT.
    LAMBDA, EPS, HP, FM, F2, LO, PU, PQ, PO, SM, SQ, TOL, UP, D50, As, Beta: Extended;
    D,S,SO,CR,Luz,C,CO,F,FI,V1,V2,RI,UI,OS,OI,PartR,PartS:VECTOR:
    Nome, Dados: String[10];
    Filedatain:text;
    P,X,V,DM,H:PARAM;
    FO:RESIDUO;
    A,XA:ARRAY[1..25] of Extended;
    FJ:ARRAY[1..40,1..8] of Extended;
    RESULT: text;
 FUNCTION FNP(X:Extended):Extended;
      BEGIN
         FNP:=SQRT(X*X+1)+X;
      END:
 FUNCTION FNX(P:Extended):Extended;
      BEGIN
         FNX:=(P*P-1)*0.5/P;
      END:
 PROCEDURE CUMULANTE(V1: Vector; Var V2: Vector);
 VAR i:integer;
   Soma:Real;
 BEGIN
   Soma:=0;
   For i:=1 to n do
    Begin
       Soma:=Soma+V1[i];
      Infra:=1-Soma;
       V2[i]:=Soma;
    End;
    V2[1]:=Soma+Infra;
    For i:=2 to n do
     V2[i]:=V2[i-1]-V1[i-1];
 END;
PROCEDURE PARTICAO (Beta:Real; V2, V3: Vector; Var V4: Vector);
 VAR i:integer;
```

```
x:PARAM;
 BEGIN
    For i:=1 to NP do x[i]:=FNP(P[i]);
   d50:=x[1]; m1:=x[2]; As:=x[3];
    CICLONAGEM(Luz,FLAG,PartS);
    Clrscr:
    gotoxy(1,5);
    Writeln('D50= ',D50:6:4,' m1= ',m1:6:4,' As= ',As:6:4);
     For j:=1 to n do
     F[j]:=PartS[j]-PartR[j];
 END;
 PROCEDURE RESULTADOS:
 BEGIN
   clrscr:
   SIMULADOR(P,F);
   clrscr:
                        RESULTADOS DA OPTIMIZAÇÃO');
   Write('
Writeln('=
                D50=',D50:10:5,'
                                   m1=',m1:10:5,' As=',As:10:5);
   Writeln('
Writeln('=
                   =');
   Writeln('
                                 Partição(Real)
                                                   Partição(Simul.)');
               LUZ(mm)
   For i:=1 to n do
    Begin
                                      ',PartR[i]:10:4,'
                                                             ',PartS[i]:10:4);
       Writeln(' ',LUZ[i]:10:4,'
    End;
Write('=
                 =');
   ReadIn:
   Begin
      clrscr;
      Writeln(' Nome do ficheiro para guardar resultados?');Readln(Dados);
      Assign(result, Dados):
      rewrite(result);
      writeIn(result,D50:8:4,m1:8:4,As:8:4);
      For i:=1 to n do
      writeln(result,luz[i]:12:5,PartR[i]:12:5,PartS[i]:12:5);
      close(result);
      end:
   ReadIn:
```

END;

```
2:BEGIN Writeln('Nov. alor de Corte=
                                          '):ReadIn(Corte):D50:=(Corte):END:
     3:BEGIN Writeln('Nov: alor de As=
                                        '):ReadIn(As);END:
     4:BEGIN Writeln('Nov: alor de D50=
                                         ');Readin(D50);END;
     5:BEGIN
         Writeln(' ExponentisSum (Lynch & Rao).....(1)');
         Writeln(' Rosin Ramter(Plitt).....(2)');
         Writeln(' Logistic(Loe & Plitt).....(3)');
        Writeln(' Escolha an ino de Modelo: '); Readln(Flag);
      END:
     6:CICLONAGEM( Luz., AG, PartS);
     7:Goto 10;
     0:EXIT:
  End:
  until 1\ightarrow1;
              {*ROTINA MRQUARDT*}
10:READLN;
  P[1]:=D50;P[2]:=m1;P[3]:=s:
  Writeln('P[1]=
                 ',P[1]:7:5
  Writeln('P[2]=
                  ',P[2]:7:5
  Writeln(P[3]=
                  ',P[3]:7:5
  readln:
 clrscr;
 N:=i;
 M:=N-2;
 NP:=3:
 NN:=TRUNC((NP+1)*NP/2
 BEGIN
   FOR I:=1 TO NP DO
    BEGIN
       H[[]:=0;
       P[I]:=FNX(P[I]);
    END;
  20:TOL:=0.00001;
   UP:=10:
   DOWN:=0.1:
   LAMBDA:=1;
   EPS:=0.001:
   SIMULADOR(P,F);
   SM:=0;
   SQ:=0;
   FOR I:=1 TO M DO
    BEGIN
      FO[[]:=F[]];
      F2:=F[I]*F[I];
      SQ:=SQ+F2:
      SM:=SM+F2*F2
    END:
   PU:=SM;
   PQ:=SQ;
   WRITELN;
   WRITELN:
  WRITELN(LAMBDA.Pt.)
 30:LAMBDA:=DOWN*LA1BDA;
 PO:=PO:
```

```
FOR JX:=1 TO NP DO
 BEGIN
   PJ:=P[JX]:
   HP:=ABS(PJ)*EPS+EPS:
   P[JX]:=PJ+HP;
   SIMULADOR(P.F):
   P[JX]:=PJ:
   FOR IX:=1 TO M DO FJ[IX,JX]:=(F[IX]-FO[IX])/HP;
 END:
JK:=0:
FOR J:=1 TO NP DO
 BEGIN
   SM:=0:
   FOR I:=1 TO M DO SM:=FJ[I,J]*FO[I]+SM:
   V[J]:=SM;
   FOR K:=1 TO J DO
    BEGIN
       JK:=JK+1;
       SM:=0:
       FOR I:=1 TO M DO SM:=FJ[I,K]*FJ[I,J]+SM;
      XA[JK]:=SM
    END:
 END:
FOR J:=1 TO NP DO DM[J]:=P[J];
40:FOR K:=1 TO NN DO A[K]:=XA[K];
  FOR J:=1 TO NP DO
   BEGIN
     KK:=TRUNC((J+1)*J/2);
     A[KK]:=XA[KK]+LAMBDA;
     X[J] := -V[J]
   END;
  FOR J:=1 TO NP DO
   BEGIN
     KK:=TRUNC((J+1)*J/2);
     IF J=1 THEN GOTO 50;
     FOR I:=J TO NP DO
      BEGIN
        IJ:=TRUNC((I-1)*I/2+J);
         SM:=A[IJ];
        FOR K:=1 TO J-1 DO SM:=SM-A[IJ-K]*A[KK-K];
         A[IJ]:=SM
      END;
    50:IF A[KK]<=0 THEN GOTO 60:
     SM:=SQRT(A[KK]):
     FOR I:=J TO NP DO
      BEGIN
        IJ:=TRUNC((I-1)*I/2+J):
        A[IJ]:=A[IJ]/SM:
      END:
   END:
  X[1]:=X[1]/A[1];
  KK:=I;
  FOR I:=2 TO NP DO
   BEGIN
     FOR J:=1 TO I-1 DO
      BEGIN
        KK:=KK+1:
        X[I]:=X[I]-A[KK]*X[J]
```

```
END:
        KK:=KK+1:
        X[I]:=X[I]/A[KK]
      END:
     X[NP]:=X[NP]/A[NN];
     I:=NP:
     REPEAT
        KK:=TRUNC((I-1)*I/2);
        FOR J:=1 TO I-1 DO X[J]:=X[J]-X[I]*A[KK+J];
        X[I-1]:=X[I-1]/A[KK];
        I:=I-1;
     UNTIL I<2;
     KOUNT:=0;
     FOR I:=1 TO NP DO
      BEGIN
        P[I]:=DM[I]+X[I];
        IF P[I]=DM[I] THEN KOUNT:=KOUNT+1
               ELSE END:
     IF KOUNT=NP THEN
     BEGIN
       RESULTADOS:
       EXIT;
     END:
     SIMULADOR(P,F);
     SM:=0;
     SQ:=0;
     FOR I:=1 TO M DO
      BEGIN
        FO[I]:=F[I];
        F2:=F[I]*F[I];
        SQ:=SQ+F2;
        SM:=SM+F2*F2
      END;
     PU:=SM;
     PQ:=SQ;
     WRITELN;
     WRITELN:
     WRITELN(LAMBDA.PQ);
     IF PQ<PO THEN GOTO 30;
   60:LAMBDA:=UP*LAMBDA;
     IF LAMBDA=0 THEN LAMBDA:=TOL:
     GOTO 40;
 END:
END.
```

```
PROGRAM APCV1(INPUT,OUTPUT,RESULT):
USES wincrt:
TYPE VECTOR = Array [1..20] of Extended;
VAR i.i.k.n.op.FLAG:integer:
   m1,m2,m3,R,U,AUX,ALM1,ALM2,ALM3,SUP1,SUP2,SUP3,SUP4,INF1,INF2,INF3,
   INF4,D501,D502,D503,As1,As2,As3,dc501,dc502,dc503,b501,b502,b503,
   dcAs1,dcAs2,dcAs3,bAs1,bAs2,bAs3,Rp1,Rp2,Rp3,Infra,Soma:Extended;
   Luz, CUMI1, F, ALMI1, ALMI2, ALMI3, SUPI1, SUPI2, SUPI3, SUPI4, INFI1, INFI2, INFI3,
   INFI4,QSUPI1,QSUPI2,QSUPI3,QSUPI4,QINFI1,QINFI2,QINFI3,QINFI4,PartS1,
   PartS2, PartS3, PartS4, V1, V2, AUXI: VECTOR;
   Nome, Dados: String[10];
   Filedatain, result: text;
PROCEDURE VINTEPOLEGADAS (Luz:Vector:FLAG:INTEGER: Var PartS1:Vector):
VAR
  i:integer;
  xi:Extended;
BEGIN
  For i:=1 to n do
     Begin
        xi:=(Luz[i]/D501);
     Case FLAG of
    1: PartS1[i]:=(As1+(1-As1)*(EXP(m1*xi)-1)/(EXP(m1*xi)+EXP(m1)-2)):
    2: PartS1[i]:=(((1-EXP(-0.693*EXP(m1*ln(xi))))*(1-AS1))+As1);
    3: PartS1[i] := (((1/(1+EXP(m1*ln(1/xi))))*(1-As1))+As1);
     End:
     End;
END;
PROCEDURE QUATORZEPOLEGADAS (Luz: Vector; FLAG: INTEGER; Var PartS2: Vector);
VAR
  i:integer;
  xi:Extended:
BEGIN
  For i:=1 to n do
     Begin
        xi:=(Luz[i]/D502);
     Case FLAG of
   1: PartS2[i]:=(As2+(1-As2)*(EXP(m2*xi)-1)/(EXP(m2*xi)+EXP(m2)-2));
   2: PartS2[i]:=(((1-EXP(-0.693*EXP(m2*ln(xi))))*(1-AS2))+As2);
   3: PartS2[i]:=(((1/(1+EXP(m2*ln(1/xi))))*(1-As2))+As2);
    End;
    End:
```

```
END;
PROCEDURE DORR (Luz: Vector; Var PartS3: Vector);
VAR
 i:integer;
  xi:Extended;
BEGIN
   For i = 1 to n do
     Begin
        PartS3[1]:=1.00;
        PartS3[2]:=1.00;
        PartS3[3]:=1.00;
        PartS3[4]:=1.00;
        PartS3[5]:=0.9963;
        PartS3[6]:=0.8725;
        PartS3[7]:=0.2092;
        PartS3[8]:=0.2915;
        PartS3[9]:=0.4081;
        PartS3[10]:=0.4785;
        PartS3[11]:=0.5392;
        PartS3[12]:=0.6052;
        PartS3[13]:=0.6634;
        PartS3[14]:=0.6996;
        PartS3[15]:=0.7217;
        PartS3[16]:=0.7345;
        PartS3[17]:=0.7351;
        PartS3[18]:=0.7290;
        PartS3[19]:=0.7106;
     End;
END;
   PROCEDURE CRIVO (Luz: Vector; FLAG: INTEGER; Var PartS4: Vector);
VAR
  i:integer;
  xi:Extended:
BEGIN
  For i:=1 to n do
     Begin
        xi:=(Luz[i]/D503);
     Case FLAG of
    1: PartS4[i]:=(As3+(1-As3)*(EXP(m3*xi)-1)/(EXP(m3*xi)+EXP(m3)-2));
   2: PartS4[i]:=(((1-EXP(-0.693*EXP(m3*ln(xi))))*(1-AS3))+As3);
   3: PartS4[i]:=(((1/(1+EXP(m3*ln(1/xi))))*(1-As3))+As3);
     End;
     End;
```

END;

```
PROCEDURE FECHADO;
 VAR i,j,k:integer;
   TESTE:Real;
BEGIN
   SUP1:=0;SUP2:=0;SUP3:=0;INF1:=0;INF2:=0;INF3:=0;INF4:=0;ALM2:=0;ALM3:=0;
   For i:=1 to n do
    Begin
      SUPI1[i]:=0;
      INFI1[i]:=0;
      SUPI2[i]:=0;
      INFI2[i]:=0;
      SUPI3[i]:=0;
      INFI3[i]:=0;
      SUPI4[i]:=0;
      INFI4[i]:=0;
    End;
    clrscr;
    Repeat
    AUX:=ALM2;
    VINTEPOLEGADAS(LUZ,Flag,PartS1);
       SUP1:=0;INF1:=0;ALM2:=0;QINFI1[i]:=0;QSUPI1[i]:=0;INFI1[i]:=0;SUPI1[i]:=0;
       ALM2:=ALM1+INF3+INF4;
      For i:=1 to n do
         ALMI2[i]:=(ALM1*ALMI1[i]+INF3*INFI3[i]+INF4*INFI4[i])/(ALM1+INF3+INF4);
{alimentação ciclone 20"}
        For j:=1 to n do
          Begin
             QINFI1[j]:=ALM2*ALMI2[j]*(1-PartS1[j]); {*UNDERFLOW20"*}
             INF1:=INF1+QINFI1[j];
                                                     {*SUPRA20"*}
             QSUPI1[j]:=ALM2*ALMI2[j]*PartS1[j];
             SUP1:=SUP1+QSUPI1[j];
          End;
        For j:=1 to n do
          Begin
            INFI1[j]:=QINFI1[j]/INF1;
             SUPI1[j]:=QSUPI1[j]/SUP1;
          End;
       Rp1:=SUP1/ALM2;
       D501:=dc501*Rp1+b501; {*CÁLCULO DE As E D50 DO CICLONE DE 20"*}
        As1:=dcAs1*Rp1+bAs1;
```

QUATORZEPOLEGADAS(LUZ,Flag,PartS2);

```
OINFI2[i]:=0;QSUPI2[i]:=0;INF2:=0;SUP2:=0;INFI2[i]:=0;SUPI2[i]:=0;
           For j:=1 to n do
                     Begin
                           INF2:=INF2+QINFI2[i];
                                                                                                                             {*SUPRA14"*}
                           QSUPI2[i]:=INF1*INFI1[j]*PartS2[j];
                           SUP2:=SUP2+QSUPI2[j];
                     End;
           For j:=1 to n do
                Begin
                         INFI2[j]:=QINFI2[j]/INF2;
                         SUPI2[j]:=QSUPI2[j]/SUP2;
                End:
          Rp2:=SUP2/INF1;
          D502:=dc502*Rp2+b502; {*CÁLCULO DE As E D50 DO CICLONE DE 14"*}
          As2:=dcAs2*Rp2+bAs2;
           DORR(Luz,PartS3);
             QINFI3[i]:=0;QSUPI3[i]:=0;INF3:=0;SUP3:=0;INFI3[i]:=0;SUPI3[i]:=0;
             For j:=1 to n do
                     Begin
                           QINFI3[j]:=SUP1*SUPI1[j]*(1-PartS3[j]); {*UNDERFLOW DORR*}
                           INF3:=INF3+QINFI3[i];
                           QSUPI3[j]:=SUP1*SUPI1[j]*PartS3[j];
                                                                                                                               {*SUPRA DORR*}
                           SUP3:=SUP3+QSUPI3[i];
                     End;
           For j:=1 to n do
                 Begin
                          INFI3[j]:=QINFI3[j]/INF3;
                          SUPI3[j]:=QSUPI3[j]/SUP3;
                 End;
        CRIVO (LUZ,Flag,PartS4);
ALM3 := 0; ALMI3[i] := 0; QINFI4[i] := 0; QSUPI4[i] := 0; INF4 := 0; SUP4 := 0; INFI4[i] := 0; SUPI4[i] := 0; ALMI3[i] := 0;
            ALM3:=SUP3+SUP2;
           For i:=1 to n do
                      ALMI3[i]:=(SUP3*SUPI3[i]+SUP2*SUPI2[i])/ALM3; {*ALIMENTAÇÃO CRIVO*}
           For j:=1 to n do
                     Begin
                           QINFI4[j]:=ALM3*ALMI3[j]*(1-PartS4[j]); {*UNDERFLOW CRIVO*}
                            INF4:=INF4+QINFI4[j];
                                                                                                                                    {*SUPRA CRIVO*}
                            QSUPI4[j]:=ALM3*ALMI3[j]*PartS4[j];
                            SUP4:=SUP4+QSUPI4[j];
                     End;
```

```
Begin
           INFI4[i]:=QINFI4[i]/INF4;
           SUPI4[i]:=QSUPI4[i]/SUP4;
       End:
    Rp3:=SUP4/ALM3:
    D503:=dc503*Rp3+b503; {*CÁLCULO DE As E D50 DO CRIVO*}
    As3:=dcAs3*Rp3+bAs3:
  clrscr:
  gotoxy(1,1);
  Writeln('
                       RESULTADOS FINAIS'):
Writeln('=
                   ='):
  Writeln(' Caudal de Alimentação(tn/h)=',ALM1:5:3,'
                                                        Caudal do Tanque(tn/h)=',ALM2:5:3);
  Writeln:
  Writeln(' Caudal de Infra 20"=',INF1:5:3,'
                                                   Caudal de Supra 20"=',SUP1:5:3);
  Writeln:
  Writeln(' Caudal de Infra 14"=',INF2:5:3,'
                                                   Caudal de Supra 14"=',SUP2:5:3);
  Writeln:
                                                     Caudal de Supra do DORR=',SUP3:5:3);
  Writeln(' Caudal de Infra do DORR=',INF3:6:5,'
  Writeln:
                                                   Caudal de Supra do Crivo=',SUP4:5:3);
  Writeln(' Caudal de Infra do Crivo=',INF4:7:3,'
  Writeln:
  Writeln(' Caudal de Retorno=',(INF3+INF4):7:3);
  Writeln;
  Writeln(' Rp1=',Rp1:8:4,'
                             Rp2=',Rp2:8:4,'
                                                   Rp3=',Rp3:8:4);
Writeln('=
                   =');
 Clrscr;
 Gotoxy(1,1);
 Writeln('
                        ALIMENTAÇÃO
                                            TANQUE
                                                         PRODUTO FINAL
                                                                               AREIAS');
                Luz
 For k:=1 to n do
 Writeln(' ',Luz[k]:8:3,' ',100*ALMI1[k]:8:3,'
                                                    ',100*ALMI2[K]:8:3,'
                                                                            ',INFI2[k]*100:8:4,
       ',SUPI4[k]*100:8:4);
Writeln('=
 UNTIL(ABS(AUX-ALM2)<0.0000000000000000001);
 Repeat until keypressed;
 Readln;
    Begin
      clrscr;
      Writeln('Nome do ficheiro para guardar resultados?'); Readln(Dados);
      Assign(result, Dados);
      rewrite(result);
      writeln(result, 'ALM20"=', ALM2:6:3,' ALIM14"= ',INF1:10:4,' INFRA14"= ',INF2:10:4,'
SUPRA14"= ',SUP2:8:4);
      writeln(result, 'SUPRA20"=',SUP1:6:4,' INFRADORR=',INF3:10:4,' SUPRADORR=
',SUP3:10:4);
```

For i:=1 to n do

```
writeln(result, 'ALMCRI"=', ALM3:6:4,' INFRACRIVO=', INF4:10:4,'
SUPRACRIVO=',SUP4:10:4);
       writeln(result,' ');
       Writeln(result, 'D501=', d501:6:5.'
                                          D502=',d502:10:5,'
                                                                   D503=',D503:10:5);
       Writeln(result, 'm1=', m1:6:5,'
                                         m2=',m2:8:5,'
                                                                m3=',m3:10:5);
       Writeln(result, 'As1=', As1:6:5,'
                                         As2=',As2:8:5,'
                                                                As3=',As3:10:5);
       writeln(result, LUZ ALM20" INF20" SUP20" INF14" SUP14" INFDORR SUPDORR
ALMCRIVO INFCRIVO SUPCRIVO');
      For i:=1 to n do
       writeln(result,luz[i]:5:3,",ALMI2[i]:8:3,",INFI1[i]:8:3,",SUPI1[i]:8:4,' ',INFI2[i]:8:4,
       ",SUPI2[i]:8:4,' ',INFI3[i]:8:4,' ',SUPI3[i]:8:4,",ALMI3[i]:8:4,' ',INFI4[i]:8:4,
       ' ',SUPI4[i]:8:4);
      close(result):
       end;
   Readln;
 END:
                     { ROTINA PRINCIPAL }
 BEGIN
   Writeln(' Número de Lotes Granulométricos: '); Readln(n);
   Writeln(' Nome do Ficheiro de Dados?
                                             ');ReadIn(Nome);
   Assign(filedatain, Nome);
   Reset(filedatain);
   i:=0:
   clrscr;
Writeln:
                    DISTRIBUIÇÃO GRANULOMÉTRICA INICIAL');
Writeln('
Writeln;
Writeln('=
                   =');
Writeln;
                                                        ','Cumulante');
Writeln('
                 Luz(mm)','
                                    ','Histograma','
Writeln;
   i:=i+1;
   For i:=1 to n do
       ReadIn(Filedatain,Luz[i],ALMI1[i],CUMI1[i]);
    End;
Begin
For i:=1 to n do
                                    ',ALMI1[i]:8:4,'
                                                          ',CUMI1[i]:8:4);
Writeln('
                 ',Luz[i]:8:4,'
End:
Writeln;
Readln;
ALM1:=1;Flag:=1;m1:=2.09531;m2:=2.09932;m3:=0.62311;D501:=0.15482;D502:=0.07773;
D503 := 0.29669; As1 := 0.3878; As2 := 0.20077; As3 := 0.78788; dc501 := -1.057471;
```

```
dc502:=-0.4463;dc503:=-0.7508;b501:=1.016994;b502:=0.2446;b503:=1.0253;
dcAs1:=1.201149;dcAs2:=0.5237;dcAs3:=2.5716;bAs1:=-0.576930;bAs2:=-0.0200;bAs3:=-1.6520;
Repeat
clrscr;
Writeln:
          PARÂMETROS DO MODELO ');
Writeln('
                                           '):
Writeln('-
                                     (1)');
Writeln('
          m1:= ', m1:3:4,'
          m2:= '.m2:3:4,'
                                     (2)');
Writeln('
          m3:= ',m3:3:4,'
                                     (3)');
Writeln('
          As1:= ',As1:3:4,'
                                     (4)');
Writeln('
          As2:= ',As2:3:4,'
                                     (5)');
Writeln('
          As3:= ',As3:3:4,'
Writeln('
                                     (6)');
          D501:= ',D501:2:4.'
Writeln('
                                       (7)');
          D502:= ',D502:2:4,'
                                        (8)');
Writeln('
          D503:= ',D503:2:4,'
                                        (9));
Writeln('
          Caudal de Alimentação(tn/h):= ',ALM1:2:4,' (10)');
Writeln('
Writeln:
          TIPO DE SIMULAÇÃO');
Writeln('
                                         =');
Writeln('=
Writeln;
Writeln(' Escolha do Modelo de Ciclonagem..... (11)');
Writeln(' SIMULAÇÃO..... (12)');
Writeln(' Terminar.....(0)');
Writeln;
Repeat
 Writeln(' ESCOLHA O PROCEDIMENTO DESEJADO -> ');Readln(op);
 until (op>=0) and (op<=13);
 GOTOXY(1,22);
     case op of
                                               '):Readln(m1);END;
      1:BEGIN Writeln('Novo Valor de m/20"=
                                               '):Readln(m2);END;
      2:BEGIN Writeln('Novo Valor de m/14"=
                                                 ');Readln(m3);END;
      3:BEGIN Writeln('Novo Valor de m/Crivo=
                                                ');Readin(As1);END;
      4:BEGIN Writeln('Novo Valor de As/20"=
      5:BEGIN Writeln('Novo Valor de As/14"=
                                                '):Readln(As2);END;
      6:BEGIN Writeln('Novo Valor de As/Crivo=
                                                 '):ReadIn(As3);END;
                                                 '):Readln(D501);END;
      7:BEGIN Writeln('Novo Valor de D50/20"=
      8:BEGIN Writeln('Novo Valor de D50/14"=
                                                 '):Readln(D502);END;
                                                   ');Readln(D503);END;
      9:BEGIN Writeln('Novo Valor de D50/Crivo=
                                                      ');Readln(ALM1);END;
      10:BEGIN Writeln('Novo Valor da Alimentação=
      11:BEGIN
          Writeln('Exponential Sum (Lynch & Rao).....(1)');
          Writeln('Rosin Rammler(Plitt).....(2)');
          Writeln('Logistic(Lilge & Plitt).....(3)');
                                                '); Readin(Flag);
          Writeln(' Escolha do Tipo de Modelo:
       END;
      12:FECHADO;
      0:EXIT;
   End;
    until 1<1;
   END.
```

```
PROGRAM APCV2(INPUT, OUTPUT, RESULT):
USES wincrt;
TYPE VECTOR = Array [1..20] of Extended;
VAR i,j,k,n,op,FLAG:integer;
   m1,m2,m3,Corte,R,U,AUX,ALM1,ALM2,ALM3,SUP1,SUP2,SUP3,SUP4,INF1,INF2,INF3,
   INF4,D501,D502,D503,As1,As2,As3,Infra,Soma:Extended;
   Luz, CUMI1, F, ALMI1, ALMI2, ALMI3, SUPI1, SUPI2, SUPI3, SUPI4, INFI1, INFI2, INFI3.
   INFI4,QSUPI1,QSUPI2,QSUPI3,QSUPI4,QINFI1,QINFI2,QINFI3,QINFI4,PartS1.
   PartS2, PartS3, PartS4, V1, V2, AUXI: VECTOR:
   Nome, Dados: String[10];
   Filedatain, result: text;
PROCEDURE VINTEPOLEGADAS (Luz: Vector; FLAG: INTEGER; Var PartS1: Vector);
VAR
  i:integer;
  xi:Extended;
BEGIN
  For i:=1 to n do
     Begin
        xi:=(Luz[i]/D501);
     Case FLAG of
   1: PartS1[i] := (As1 + (1-As1) + (EXP(m1 + xi) - 1)/(EXP(m1 + xi) + EXP(m1) - 2));
   2: PartS1[i] := (((1-EXP(-0.693*EXP(m1*ln(xi))))*(1-AS1))+As1);
   3: PartS1[i] := (((1/(1+EXP(m1*ln(1/xi))))*(1-As1))+As1);
    End;
    End:
END;
PROCEDURE QUATORZEPOLEGADAS (Luz: Vector; FLAG: INTEGER; Var PartS2: Vector);
VAR
 i:integer;
 xi:Extended;
BEGIN
  For i:=1 to n do
    Begin
        xi:=(Luz[i]/D502);
    Case FLAG of
   1: PartS2[i]:=(As2+(1-As2)*(EXP(m2*xi)-1)/(EXP(m2*xi)+EXP(m2)-2));
   2: PartS2[i]:=(((1-EXP(-0.693*EXP(m2*ln(xi))))*(1-AS2))+As2);
   3: PartS2[i]:=(((1/(1+EXP(m2*ln(1/xi))))*(1-As2))+As2);
    End;
    End;
```

END;

```
PROCEDURE DORR (Luz: Vector; Var PartS3: Vector);
VAR
  i:integer;
  xi:Extended;
BEGIN
   For i = 1 to n do
      Begin
        PartS3[1]:=1.0000;
        PartS3[2]:=1.0000;
        PartS3[3]:=1.0000;
        PartS3[4]:=1.0000;
        PartS3[5]:=0.9963;
        PartS3[6]:=0.8725;
        PartS3[7]:=0.2092;
        PartS3[8]:=0.2915;
        PartS3[9]:=0.2915;
        PartS3[10]:=0.2915;
        PartS3[11]:=0.2915;
        PartS3[12]:=0.2915;
        PartS3[13]:=0.2915;
        PartS3[14]:=0.2915;
        PartS3[15]:=0.2915;
        PartS3[16]:=0.2915;
        PartS3[17]:=0.2915;
        PartS3[18]:=0.2915;
        PartS3[19]:=0.2915;
     End;
END;
   PROCEDURE CRIVO (Luz: Vector; FLAG: INTEGER; Var PartS4: Vector);
VAR
 i:integer;
  xi:Extended;
BEGIN
  For i:=1 to n do
    Begin
        xi:=(Luz[i]/D503);
     Case FLAG of
   1: PartS4[i]:=(As3+(1-As3)*(EXP(m3*xi)-1)/(EXP(m3*xi)+EXP(m3)-2));
   2: PartS4[i]:=(((1-EXP(-0.693*EXP(m3*ln(xi))))*(1-AS3))+As3);
   3: PartS4[i]:=(((1/(1+EXP(m3*ln(1/xi))))*(1-As3))+As3);
    End;
    End;
```

```
PROCEDURE FECHADO;
 VAR i,j,k:integer;
   TESTE:Real;
 BEGIN
   SUP1:=0;SUP2:=0;SUP3:=0;INF1:=0;INF2:=0;INF3:=0;INF4:=0;ALM2:=0;ALM3:=0;
   For i:=1 to n do
    Begin
      SUPI1[i]:=0;
      INFI1[i]:=0;
      SUPI2[i]:=0;
      INFI2[i]:=0;
      SUPI3[i]:=0;
      INFI3[i]:=0;
      SUPI4[i]:=0;
      INFI4[i]:=0;
    End;
    clrscr;
    Repeat
       AUX:=ALM2;
    VINTEPOLEGADAS(LUZ,Flag,PartS1);
       SUP1:=0;INF1:=0;
       ALM2:=ALM1+INF3+INF4;
      For i:=1 to n do
        ALMI2[i]:=(ALM1*ALMI1[i]+INF3*INFI3[i]+INF4*INFI4[i])/(ALM1+INF3+INF4);
{alimentação ciclone 20"}
         For j:=1 to n do
          Begin
             QINFI1[j]:=ALM2*ALMI2[j]*(1-PartS1[j]); {*UNDERFLOW20**}
             INF1:=INF1+QINFI1[j];
             QSUPI1[j]:=ALM2*ALMI2[j]*PartS1[j];
                                                     {*SUPRA20"*}
             SUP1:=SUP1+QSUPI1[j];
          End;
        For j:=1 to n do
             INFI1[j]:=QINFI1[j]/INF1;
             SUPI1[j]:=QSUPI1[j]/SUP1;
          End;
    QUATORZEPOLEGADAS(LUZ,Flag,PartS2);
    INF2:=0;SUP2:=0;
    For j:=1 to n do
       Begin
```

```
QINFI2[i]:=INF1*INFI1[i]*(1-PartS2[i]); {*UNDERFLOW14"*}
      INF2:=INF2+OINFI2[i]:
      OSUPI2[i]:=INF1*INFI1[i]*PartS2[i]:
                                          {*SUPRA14"*}
      SUP2:=SUP2+QSUPI2[i];
    End;
For j:=1 to n do
  Begin
     INFI2[j]:=QINFI2[j]/INF2;
     SUPI2[j]:=QSUPI2[j]/SUP2;
  End:
DORR(Luz, PartS3);
INF3:=0;SUP3:=0;
For j:=1 to n do
    Begin
      QINFI3[j]:=SUP1*SUPI1[j]*(1-PartS3[j]); {*UNDERFLOW DORR*}
      INF3:=INF3+QINFI3[j];
      OSUPI3[i]:=SUP1*SUPI1[i]*PartS3[i];
                                            {*SUPRA DORR*}
      SUP3:=SUP3+QSUPI3[j];
    End;
For j:=1 to n do
  Begin
     INFI3[j]:=QINFI3[j]/INF3;
     SUPI3[j]:=QSUPI3[j]/SUP3;
  End;
CRIVO (LUZ,Flag,PartS4);
INF4:=0;SUP4:=0;
ALM3:=SUP3+SUP2;
For i:=1 to n do
    ALMI3[i]:=(SUP3*SUPI3[i]+SUP2*SUPI2[i])/ALM3; {*ALIMENTAÇÃO CRIVO*}
For j:=1 to n do
   Begin
      QINFI4[j]:=ALM3*ALMI3[j]*(1-PartS4[j]); {*UNDERFLOW CRIVO*}
      INF4:=INF4+QINFI4[i];
      QSUPI4[j]:=ALM3*ALMI3[j]*PartS4[j];
                                              {*SUPRA CRIVO*}
      SUP4:=SUP4+QSUPI4[j];
   End;
For j:=1 to n do
  Begin
     INFI4[j]:=QINFI4[j]/INF4;
     SUPI4[j]:=QSUPI4[j]/SUP4;
  End;
```

```
end;
    Readin:
 END:
                      { ROTINA PRINCIPAL }
 BEGIN
   clrscr:
    Writeln(' Número de Lotes Granulométricos: '); Readln(n);
    Writeln(' Nome do Ficheiro de Dados?
                                               ');ReadIn(Nome);
    Assign(filedatain, Nome);
   Reset(filedatain):
   i:=0;
   clrscr;
Writeln;
                     DISTRIBUIÇÃO GRANULOMÉTRICA INICIAL');
Writeln('
Writeln;
Writeln('
                    =');
Writeln:
Writeln('
                  Luz(mm)','
                                     ','Histograma','
                                                         ','Cumulante');
Writeln;
   i:=i+1;
   For i:=1 to n do
    Begin
       Readln(Filedatain,Luz[i],ALMI1[i],CUMI1[i]);
    End:
Begin
For i:=1 to n do
Writeln('
                  ',Luz[i]:8:4,'
                                      ',ALMI1[i]:8:4,'
                                                            ',CUMI1[i]:8:4);
End;
Writeln;
Readin:
ALM1:=1:Flag:=1:m1:=2.09531;m2:=2.09932;m3:=0.62311;D501:=0.06886;D502:=0.22095;
D503:=0.30018;As1:=0.50003;As2:=0.00775;As3:=0.83165;
Repeat
clrscr;
Writeln;
           PARÂMETROS DO MODELO ');
Writeln('
Writeln('=
           m1:= ',m1:3:4,'
m2:= ',m2:3:4,'
                                        (1)');
Writeln('
Writeln('
                                        (2)');
           m3:= ',m3:3:4,'
                                        (3));
Writeln('
           As1:= ',As1:3:4.'
Writeln('
                                         (4)');
Writeln('
           As2:= ',As2:3:4,'
                                         (5)');
           As3:= ',As3:3:4,'
                                         (6)');
Writeln('
Writeln('
          D501:= ',D501:2:4,'
                                           (7)');
                                           (8)');
Writeln(' D502:= ',D502:2:4,'
          D503:= ',D503:2:4,'
                                           (9)');
Writeln('
          Caudal de Alimentação(tn/h):= ',ALM1:2:4,' (10)');
Writeln('
Writeln:
```

```
clrscr;
  gotoxy(1,1);
  Writeln('
                        RESULTADOS FINAIS'):
Writeln('=
                    ='):
  Writeln(' Caudal de Alimentação(tn/h)=',ALM1:5:3,'
                                                         Caudal do Tanque(tn/h)=',ALM2:5:3);
  Writeln;
                                                   Caudal de Supra 20"=',SUP1:5:3);
  Writeln(' Caudal de Infra 20"=',INF1:5:3,'
  Writeln;
  Writeln(' Caudal de Infra 14"=',INF2:5:3,'
                                                   Caudal de Supra 14"=',SUP2:5:3);
  Writeln:
  Writeln(' Caudal de Infra do DORR=',INF3:6:5.'
                                                     Caudal de Supra do DORR=',SUP3:5:3);
  Writeln;
  Writeln('Caudal de Infra do Crivo=',INF4:7:3.'
                                                    Caudal de Supra do Crivo='.SUP4:5:3):
  Writeln:
  Writeln(' Caudal de Retorno=',(INF3+INF4):7:3);
  Writeln:
Writeln('=
                    ·');
  Clrscr;
  Gotoxy(1,1);
  Writeln('
                 Luz
                        ALIMENTAÇÃO
                                            TANOUE
                                                          PRODUTO FINAL
                                                                                AREIAS');
  For k:=1 to n do
                                                    ',100*ALMI2[K]:8:3,'
  Writeln(' ',Luz[k]:8:3,' ',100*ALMI1[k]:8:3,'
                                                                            ',INFI2[k]*100:8:4,
        ',SUPI4[k]*100:8:4);
Writeln('=
  UNTIL(ABS(AUX-ALM2)<0.000000000000000001):
 Repeat until keypressed;
 ReadIn:
    Begin
      clrscr:
      Writeln(' Nome do ficheiro para guardar resultados?'); Readln(Dados);
      Assign(result, Dados);
      rewrite(result);
      writeln(result,'ALM20"=',ALM2:6:3,' ALIM14"= ',INF1:10:4,' INFRA14"= ',INF2:10:4,'
SUPRA14"=',SUP2:8:4);
      writeln(result, 'SUPRA20"=',SUP1:6:4,' INFRADORR=',INF3:10:4,' SUPRADORR=
',SUP3:10:4);
      writeIn(result, 'ALMCRI"=', ALM3:6:4,' INFRACRIVO=', INF4:10:4,'
SUPRACRIVO=',SUP4:10:4);
      writeln(result,' ');
      Writeln(result, 'm1=', m1:6:5,'
                                        m2=',m2:8:5,'
                                                              m3=',m3:10:5);
                                         D502=',d502:10:5,'
                                                                  D503=',D503:10:5);
      Writeln(result, 'D501=', d501:6:5,'
      Writeln(result, 'As1=', As1:6:5,'
                                        As2=',As2:8:5,'
                                                               As3=',As3:10:5);
      writeln(result,' ');
      writeln(result, LUZ ALM20" INF20" SUP20" INF14" SUP14" INFDORR SUPDORR
ALMCRIVO INFCRIVO SUPCRIVO');
      For i:=1 to n do
```

writeln(result,luz[i]:5:3,",ALMI2[i]:6:3,",INFI1[i]:8:3,",SUPI1[i]:8:4,",INFI2[i]:8:4, ",SUPI2[i]:8:4,',INFI3[i]:8:4,',SUPI3[i]:8:4,',ALMI3[i]:8:4,',INFI4[i]:8:4,

' ',SUPI4[i]:8:4); close(result);

```
Writeln(' TIPO DE SIMULAÇÃO'):
Writeln(1
                                       ='):
Writeln:
Writeln(' Escolha do Modelo de Ciclonagem..... (11)');
Writeln(' SIMULAÇÃO.....(12)');
Writeln(' Terminar....(0)');
Writeln;
Repeat
 Writeln(' ESCOLHA O PROCEDIMENTO DESEJADO > ');Readln(op);
 until (op>=0) and (op<=13);
 GOTOXY(1,22);
    case op of
     1:BEGIN Writeln('Novo Valor de m/20"=
                                             ');Readln(m1);END;
     2:BEGIN Writeln('Novo Valor de m/14"=
                                             ');Readln(m2);END;
     3:BEGIN Writeln('Novo Valor de m/Crivo=
                                              '):ReadIn(m3):END:
                                             '):Readln(As1);END;
     4:BEGIN Writeln('Novo Valor de As/20"=
     5:BEGIN Writeln('Novo Valor de As/14"=
                                              '):Readln(As2);END:
     6:BEGIN Writeln('Novo Valor de As/Crivo=
                                               ');ReadIn(As3):END:
     7:BEGIN Writeln('Novo Valor de D50/20"=
                                               ');Readln(D501);END;
     8:BEGIN Writeln('Novo Valor de D50/14"=
                                               ');Readin(D502);END;
     9:BEGIN Writeln('Novo Valor de D50/Crivo=
                                                ');ReadIn(D503);END;
     10:BEGIN Writeln('Novo Valor da Alimentação=
                                                   ');ReadIn(ALM1);END;
     11:BEGIN
        Writeln('Exponential Sum (Lynch & Rao).....(1)');
        Writeln('Rosin Rammler(Plitt).....(2)');
        Writeln('Logistic(Lilge & Plitt).....(3)');
        Writeln('Escolha do Tipo de Modelo:
                                             '); ReadIn(Flag);
      END;
     12:FECHADO;
     0:EXIT;
  End;
  until 1\ightharpoonup1;
  END.
```

ANEXO IV

RESULTADOS DAS SIMULAÇÕES

- -SIMULAÇÃO PADRÃO
- -SIMULAÇÕES DE NOVAS CONDIÇÕES OPERATÓRIAS
- -OUTRAS SIMULAÇÕES

SIMULAÇÃO PADRÃO

			SIMULA	SIMULAÇAO PADRAO	9					
1.155		ALIM14"=	0.1094	ALIM DORR=	1 0355	-igOM iA	22700			
0.1094	_	INF14"=	0.1036	INFDORR=	0.1235	INFORM	0.81/8			
1.0355		SUPRA14"=	0.0058	SUPDORR.	0.912	SUPCRIVO	0.0314			
1.0355		RP INFRA	0.1036	RECUP12µ	61.483	RECUP2µ	61,942			
Ē		2.095	m1=	2.099	m1=	0.062				
D501=	•	0.069	D\$05=	0.221	D503=	0.300				
As1=0		0.500	As2=	0.008	As3=	0.832				
ALM20"		INF20"	\$UP20"	INF14"	SUP14"	INFDORR	Suppose	On account		
0.890		1.000	1.000	1.000	1.000	1.000	1,000	1000	INFCRIVO	SUPCRIVO
0.969		1.000	0.976	1.000	1.000	1.000	0.973	0.973	3 5	30.0
0.737		1.000	0.718	1.000	1.000	1.000	0.680	0.682	8 6	0.972
0.570		1.000	0.531	1.000	1.000	1.000	0.468	0.471	986.0	0.071
0.449		90.5	0.396	1.000	1.000	1.000	0.314	0.319	0.903	0.298
350			0.294	1.000	1.000	0.997	0.199	0.204	0.722	0.186
0.230		0.998	0.174	0.999	0.978	0.869	0.080	0.086	0.396	0.075
0.178		0.824	0.112	0.840	0.547	0.457	990:0	0.069	0.324	0900
0.138		0.679	0.083	0.700	0.324	0.281	0.056	0.058	0.275	0.050
9 90		0.093	0.070	0.614	0.236	0.216	0.050	0.051	0.245	0.044
280		187.0	con	0.511	0.154	0.154	0.042	0.043	0.207	0.037
200.0		0.420	0.048	0.446	0.118	0.124	0.037	0.038	0.183	0.033
) o		0.50	0.038	0.365	0.083	0.093	0.031	0.031	0.152	0.027
8000		0.302	50.0	0.316	0.066	0.078	0.027	0.027	0.132	0.023
		0.241	0.026	0.253	0.048	0.061	0.021	0.022	0.105	0.019
0000		0.203	270.0	0.213	0.038	0.051	0.018	0.018	0.088	0.016
0.025		0.13	2 20 0	0.165	0.028	0.040	0.014	0.014	0.068	0.012
0.018		2000	2 0	0.134	0.023	0.033	0.011	0.011	0.055	0.010
		760.0	0.010	0.097	0.016	0.024	0.008	0.008	0.039	0.007

SIMULAÇÕES DE NOVAS CONDIÇÕES OPERATÓRIAS	

				SIMULAC	AO Nº 2 C	SIMULAÇÃO Nº 2 C/ As DO DORR = 30%	RR = 30%				
	_										
		ALM20"=	1.191	ALIM14"=	0.1265	ALIM DORR=	1.0544	ALMCRI*	0.8977		
		INFRA 20"	0.1265	INF14"=	0.1204	INFDORR=	0.1628	INFCRIVO	0.0281		
		SUPRA20"=	1.0544	SUPRA14"=	0.0061	SUPDORR	0.8916	SUPCRIVO	9698.0		
	- 	RP SUPRA	1.0544	RP INFRA	0.1204	RECUP12µ	78.6386	RECUP2µ	79.9072		
			m.	2.09531	m1=	2.09932	m1=	0.062311			
		•	D501=	0.06886	D502=	0.22095	D503=	0.30018			-
			As1=0	0.50003	As2=	0.00775	As3**	0.83165			
רחב	ALIM CIRC.	ALM20"	INF20"	SUP20"	INF14"	SUP14"	INFDORR	Sliphobb	Omegon IV	1	
0000	1.000	1.000	1.000	1.000	1.000	1.000	1,000	000	ALMCRIVO 1	INFCRIVO	SUPCRIVO
4.000	0.978	. 0.971	0.998	0.977	1.000	1,000	000	0.973	200.0	9 5	000
2.000	0.710	0.746	0.998	0.723	1.000	1.00	001	0.872	0.973	90.	0.972
1000	0.518	0.584	0.998	0.540	1.000	1.000	1,000	0.456	0.679	000	0.004
0.500	0.380	0.466	0.998	0.407	1.000	1.000	1.000	0.299	0808 0808	0.00	244.0
0.250	0.281	0.378	0.998	0.307	1.000	1.000	0.998	0.181	0.187	60.0	0.283
0.074	0.183	0.273	0.996	0.189	0.999	0.979	006.0	0.059	90.0	900.0 900.0	0.1.0
0.048	0.140	0.203	0.846	0.128	0.862	0.573	0.588	0.044	800.0	0.323	0.05
0.032	0.117	0.164	0.721	0.099	0.741	0.362	0.455		0.048	0.245	0.042
0.024	0.103	0.143	0.639	0.085	0.660	0.220	2	0.034	0.036	0.190	0.032
0.016	0.086	0.118	0.537	0.069	0.557	0.182	0.30	0.029	0.031	0.162	0.027
0.012	0.075	0.103	0.472	0.059	0.490	243	0.00	0.024	0.025	0.131	0.021
0.008	0.062	0.084	0.389	0.048	0.408	0.142	0.273	0.021	0.021	0.114	0.018
900.0	0.053	0.073	0.337	0.042	0 - F	0.100	0.222	0.017	0.017	0.092	0.015
0.004	0.043	0.058	0.270	60.0	1000	0.080	191.0	0.014	0.015	0.079	0.013
0.003	0.036	0.049	7660	5 6000	0.20	0.058	0.152	0.011	0.012	0.063	0.010
0.002	0.028	0.038	0.175	0.020	0.237	0.047	0.127	0.010	0.010	0.053	0.009
0.002	0.022	0.031	0.143	0.017	3 5	0.034	0.098	0.007	0.008	0.040	0.007
0.001	0.016	0.022	0.102	0.017	6 6	0.027	0.080	0.006	900.0	0.033	0.005
] . 			7100	20.0	810.0	0.057	0.004	0.004	0.024	0.004

			SIIS	SIMULAÇÃO Nº 3		C/ AS CICLONE DE 20" = 30%	DE 20" = 3	30%			
		ALM20"=	1.115	ALIM14"=	0.1335	ALIM DORR=	0.9815	A! MCRI#	2008.0		
		INFRA 20"=	0.1335	INF14"=	0.1266	INFDORR	0.0881	INFCRIVO	0.027		
		SUPRA20"=	0.9815	SUPRA14"=	0.0069	SUPDORR=	0.8934	SUPCRIVO=	0.8634		•
		RP SUPRA	0.9815	RP INFRA	0.1266	RECUP12µ	77.8985	RECUP2µ	78.8684		
		1	m1=	2.095	m1=	2.099	m1=	0.062			
		1	D501=	0.069	D502=	0.221	D503=	0.300			
			As1=0	0:300	As2=	0.008	As3=	0.832			
·				Ē							
רחב	ALIM CIRC.	ALM20"	INF20"	SUP20"	INF14"	SUP14"	INFDORR	SUPDORR	ALMCRIVO	INFCRIVO	SUBCRIVO
9:000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.00	1.000	1,000	000
4.000	0.978	0.969	1.000	0.975	1.000	1.000	1.000	0.972	0.972	1.000	0.972
2.000	0.710	0.729	1.000	0.700	1.000	1.000	1.000	0.669	0.672	1.000	0.662
1 80	0.518	0.556	1.000	0.501	1.000	1.000	1.000	0.451	0.455	0.983	0.438
0.500	0.380	0.430	1.000	0.357	1.000	1.000	1.000	0.292	0.298	0.887	0.279
0.250	0.281	0.336	1.000	0.248	1.000	1.000	966.0	0.173	0.180	0.677	0.164
0.074	0.183	0.229	0.998	0.120	0.899	0.974	0.816	0.051	0.058	0.298	0.051
0.048	0.140	0.162	0.832	0.072	0.847	0.552	0.392	0.040	0.044	0.231	0.038
0.032	0.117	0.127	0.694	0.051	0.713	0.334	0.231	0.033	0.035	0.190	0.031
0.024	0.103	0.109	0.610	0.042	0.630	0.245	0.174	0.029	0.031	0.167	0.027
0.016	0.086	0.089	0.508	0.033	0.527	0.163	0.122	0.024	0.025	0.139	0.022
0.012	0.075	0.077	0.444	0.028	0.462	0.126	0.097	0.022	0.022	0.122	0.019
800.0	0.062	0.063	0.364	0.023	0.380	0.088	0.072	0.018	0.018	0.100	0.016
9000	0.053	0.054	0.315	0.019	0.329	0.071	0.060	0.015	0.016	0.087	0.014
90.00	0.043	0.043	0.252	0.015	0.263	0.051	0.047	0.012	0.013	0.069	0.011
0.003	0.036	0.036	0.212	0.013	0.222	0.041	0.039	0.010	0.011	0.058	600.0
0.002	0.028	0.028	0.164	0.010	0.171	0.030	0.030	900.0	0.008	0.044	0.007
0.002	0.022	0.023	0.134	0.008	0.140	0.024	0.025	900.0	0.007	0.036	9000
0.001	0.016	0.016	0.096	9000	0.100	0.017	0.018	0.005	0.005	0.025	0.004

				SIMULAÇA	O Nº 4 C	SIMULAÇÃO Nº 4 C/ AS DO CRIVO = 30%	VO = 30%				
		ALM20"	1.336	ALIM14"=	0.1422	ALIM DORR=	1.1938	ALMCRI=	1.0281		
		INFRA 20"=	0.1422	INF14"=	0.1347	INFDORR=	0.163	INFCRIVO	0.1728		
		SUPRA20"=	1.1938	SUPRA14"=	0.0075	SUPDORR=	1.0308	SUPCRIVO=	0.8553		
		RP SUPRA	1.1938	RP INFRA	0.1347	RECUP12µ	81.142	RECUP2µ	81.907		
			m1=	2.095	m1=	2.099	m1=	0.062			
			D501=	690.0	D502=	0.221	D503=	0.300			
			As1=0	0.500	As2*	0.008	As3#	0.300			
	!	l					:				
רחב	ALIM CIRC.	ALM20"	INF20"	SUP20"	INF14"	SUP14"	INFDORR	SUPDORR	ALMCRIVO	INFCRIVO	SUPCRIVO
6.000	1.000	0.993	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
4.000	0.978	0.975	1.000	0.979	1.000	1.000	1.000	0.976	0.976	1.000	0.971
2.000	0.710	0.775	1.000	0.753	1.000	1.000	1.000	0.714	0.716	1.000	0.658
1.000	0.518	0.629	1.000	0.589	1.000	1.000	1.000	0.523	0.526	0.989	0.433
0.500	0.380	0.518	1.000	0.463	1.00	1.000	1.000	0.377	0.382	0.922	0.272
0.250	0.281	0.422	1.000	0.354	1.000	1.000	0.997	0.252	0.257	0.755	0.156
0.074	0.183	0.283	0.998	0.198	0.999	0.975	0.852	0.094	0.100	0.389	0.041
0.048	0.140	0.201	0.823	0.127	0.839	0.540	0.444	0.076	0.080	0.318	0.031
0.032	0.117	0.157	0.682	0.094	0.702	0.323	0.276	0.065	0.067	0.272	0.026
0.024	0.103	0.135	0.598	0.079	0.619	0.236	0.213	0.058	0.059	0.242	0.022
0.016	0.086	0.110	0.497	0.064	0.517	0.156	0.153	0.050	0.050	0.206	0.019
0 012	0.075	0.095	0.434	0.055	0.452	0.120	0.124	0.044	0.044	0.183	0.016
0.008	0.062	0.077	0.356	0.044	0.371	0.084	0.093	0.037	0.037	0.152	0.013
9000	0.053	990.0	0.308	0.038	0.322	0.067	0.078	0.032	0.032	0.132	0.012
0.004	0.043	0.052	0.246	0.030	0.257	0.049	0.061	0.025	0.025	0.105	0.009
0.003	0.036	0.044	0.207	0.025	0.217	0.039	0.051	0.021	0.021	0.088	900.0
0.002	0.028	0.034	0.160	0.019	0.167	0.029	0.040	0.016	0.016	0.068	900.0
0.002	0.022	0.028	0.131	0.016	0.137	0.023	0.033	0.013	0.013	0.055	0.005
0.001	0.016	0.020	0.094	0.011	0.098	0.016	0.024	0.009	0.00	0.039	0.003

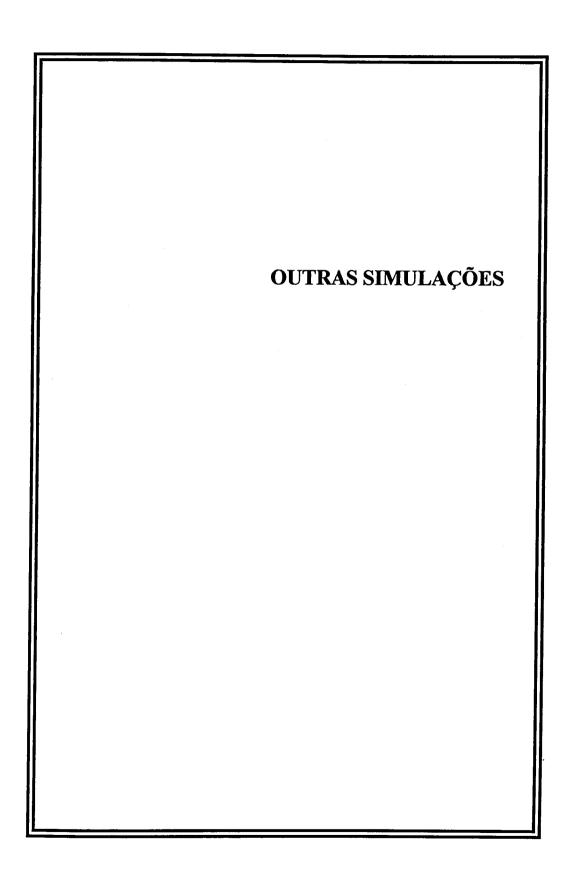
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			MIS		SIMILI ACAO NISE CADES CICI ONE DE 4411 - 45		77 - 117				
				ָּבְּיִבְּיִבְּיִבְּיִבְּיִבְּיִבְּיִבְּי			4. II. 4.				
	ALM20"=	1.165	ALIM14"=	0.1125	ALIM DORR=	1.0525	ALMCRI-	0.9526			
	INFRA 20"=	0.1125	INF14"=	0.074	INFDORR=	0.1289	INFCRIVO	0.0365			
	SUPRA20"=	1.0525	SUPRA14"=	0.0385	SUPDORR=	0.9236	\$UPCRIVO■	0.9161			
	RP SUPRA	1.0525	RP INFRA	0.074	RECUP12µ	59.4720	RECUP2µ	61.5384			
	4	m1=	2.095	m1=	2.099	m1=	0.623				
	<u>-</u>	D501=	0.069	D502=	0.040	D503#	0.300				
		As1=0	0.500	As2=	0.008	As3=	0.832				
			-								
ZNJ	ALIM CIRC.	ALM20"	INF20"	SUP20"	INF14"	SUP14"	INFDORR	SUPDORR	ALMCRIVO	INFCRIVO	SUPCRIVO
9.000	1.000	1.000	1:001	1.000	1.000	1.000	1.00	1.000	1.000	1.000	1.000
4.000	0.978	0.970	1.001	0.976	1.000	1.000	1.000	0.973	0.974	1.000	0.973
2.000	0.710	0.740	1.001	0.720	1.000	1.000	1.000	0.680	0.693	1.000	0.681
1.000	0.518	0.574	1.001	0.535	1.000	1.000	1.000	0.469	0.491	0.988	0.471
0.500	0.380	0.454	1.001	0.400	1.000	1.000	1.000	0.316	0.344	0.916	0.321
0.250	0.281	0.364	1.001	0.299	1.000	1.000	0.997	0.201	0.233	0.761	0.212
0.074	0.183	0.257	0.999	0.180	1.000	0.994	0.874	0.082	0.119	0.481	0.105
0.048	0.140	0.180	0.818	0.114	0.964	0.536	0.452	0.067	0.086	0.357	0.075
0.032	0.117	0.138	0.669	0.083	0.878	0.267	0.274	0.056	0.065	0.276	0.056
0.024	0.103	0.118	0.583	0.070	0.797	0.171	0.209	0.050	0.055	0.235	0.048
0.016	0.086	0.095	0.481	0.055	0.683	0.092	0.149	0.042	0.044	0.191	0.038
0.012	0.075	0.082	0.418	0.047	0.603	0.062	0.119	0.037	0.038	0.166	0.033
8000	0.062	990.0	0.341	0.038	0.500	0.036	0.089	0.031	0.031	0.135	0.027
9000	0.053	0.057	0.294	0.033	0.435	0.026	0.075	0.027	0.027	0.116	0.023
0.00	0.043	0.045	0.235	0.026	0.350	0.016	0.058	0.021	0.021	0.092	0.018
0.003	0.036	0.038	0.198	0.022	0.295	0.012	0.049	0.018	0.018	0.077	0.015
0.002	0.028	0.029	0.153	0.017	0.229	0.008	0.038	0.014	0.014	0.059	0.012
0.002	0.022	0.024	0.125	0.014	0.187	0.006	0.031	0.011	0.011	0.048	0.009
0.001	0.016	0.017	0:00	0.010	0.135	0.004	0.023	0.008	0.008	0.034	0.007

_								_	 		<u> </u>																			
										SUPCRIVO	1.000	0.970	0.650	0.418	2 636.0	0.433	0.134	0.016	0.009	900:0	0.005	0.00	0.004	0.003	0.003	0.002	0.002	0.001	0.001	0.001
										INFCRIVO	1.000	1.000	1.000	0.985	0.896	2 6	0.673	0.182	0.117	0.088	0.076	0.062	0.054	0.044	0.038	0.030	0.025	0.019	0.016	0.011
4		0.9626	0.1291	0.8335	96.4145					ALMCRIVO	1.000	0.975	0.697	0.494	0.340	700.0	0.207	0.039	0.024	0.018	0.015	0.012	0.011	0.009	0.007	0.006	0.005	0.004	0.003	0.002
m1 E m2 =		ALMCRIE	INTCRINO	SUPCRIVO	RECUP2µ	0.623	0.300	0.300		SUPDORR	1.000	0.974	0.695	0.492	0.337	0 203	503.0	0.035	0.021	0.016	0.014	0.011	0.010	0.008	0.007	0.005	0.004	0.003	0.003	0.002
30% E C/	4 0040	1.0919	0.1223	0.9094	95.8168	m1=	D503=	As3#	4000	INFOORK	1.000	1.000	1.000	1.000	1.000	966.0	e co	0.00	0.409	0.305	0.260	0.212	0.184	0.150	0.129	0.103	0.087	0.067	0.054	0.039
IULAÇÃO № 6 C/ As1, As3 E As DORR = 30% E C/ m1 E m2 =	ALIM DORB-	INEDORRE	-aaoualls		RECUP12μ	4.000	0.221	0.008	11044"	11.00	00.	1:000	1.000	1.000	1.000	1.000	666.0	0000	0.390	0.394	0.312	0.232	0.192	0.149	0.125	0.097	0.080	0.061	0.049	0.035
s1, As3 E /	0.1601	0.1565	0.0036		0.1565	±	D502=	As2=	INF14"	500	8 8	000.	1.000	1.000	1.000	1.000	1.000	0.845	2445	10.00	0.027	0.524	0.460	0.378	0.327	0.262	0.220	0.170	8 6	6.088
O N° 6 C/ A	ALIM14"=	INF14"=	SUPRA14"	100	AF INFRA	4.000	0.069	0.300	\$UP20"	900	7200	0.97	0.730	0.550	0.412	0.293	0.122	0.066	0.049	0.043	700	t 0000	0.030	0.024	120.0	0.017	0.014	0.00	8000	000
SIMULAÇA	1.252	0.1601	1.0919	4 0040	6160.1	Ē	D501**	As1=0	INF20"	1.000	000	2	9 9	1.000	1.000	1.000	1.000	0.839	0.704	0.620	0.518	0.454	525.0	2000	0.323	0.238	0.167	0.136	0.097	
o)	ALM20"=	INFRA 20"=	SUPRA20"=	RP SUPRA					ALM20"	1.000	0.974	0.760	0.604	5 6	0.400	0.382	0.234	0.165	0.133	0.116	960.0	0.084	6900	0900	0.048	0.040	0.031	0.025	0.018	
					-				ALIM CIRC.	1.000	0.978	0.710	0.518	0.380	9000	0.201	0.183	0.140	0.117	0 103	0.086	0.075	0.062	0.053	0.043	0.036	0.028	0.022	0.016	•
									LUZ(mm)	00009	4.000	2.000	1.000	0.500	0.250	2	0.074	0.048	0.032	0.024	0.016	0.012	0.008	900:0	0.004	0.003	0.002	0.002	0.001	

SIMULAÇAO N°7 C/AS1, AS3 E AS DORR = 30% E C/ m1 E m2 =
1.289 ALIM14"=
0.182 INF14"=
1.107 SUPRA14"
1.107 RP INFRA
m1= 4.000
D501≈ 0.069
As1=0 0.300
INF20" SUP20"
1.000
1.000 0.978
1.000 0.734
0.710 0.055
0.523 0.047
0.09 0.007

	ALM20"	1.231	ALIM14"=	0.1699	ALIM DORR=	1.0611	A! MCRI=	0.0505			
	INFRA 20"=	0.1699	iNF14"=	0.1586	INFDORR=	0.1025	INFCRIVO	0.1281			
	SUPRA20"=	1.0611	SUPRA14"=	0.0113	SUPDORR=	0.9586	SUPCRIVO=	0.8314			
	RP SUPRA	1.0611	RP INFRA	0.1586	RECUP12µ	95.48	RECUP2µ	96.27			
		m1*	2.095	m1=	2.099	m,	0.623				
		D501=	0.100	D502=	0.040	D503=	0.300				
	- 	As1=0	0.300	As2=	0.008	As3=	0.300				
		i									
רחב	ALIM CIRC.	ALM20"	INF20"	SUP20"	INF14"	SUP14"	INFDORR	SUPDORR	ALMCRIVO	OWIGCENIA	Cylanata
000.9	1.000	1,000	1.000	1.000	1.000	1.000	08-	1 000	1 000	100	
4.000	0.978	0.972	1.001	0.977	1.000	1.000	1.000	0.974	0.974	8 6	020
2.000	0.710	0.755	1.001	0.722	1.000	1.000	1.000	0.692	0.696	1.000	0.649
1.000	0.518	0.597	1.001	0.537	1.000	1.000	1.000	0.487	0.493	0.985	0.417
0.500	0.380	0.476	1.001	0.395	1.000	1.000	1.000	0.330	0.338	0.895	0.251
0.250	0.281	0.371	1.001	0.273	1.000	0.999	0.995	0.195	0.204	0.670	0.132
4,00	0.183	0.222	0.973	0.103	0.987	0.757	0.773	0:030	0.039	0.186	0.016
6 5	0.140	0.170	0.799	0.070	0.826	0.413	0.506	0.023	0.027	0.135	0.011
0.032	0.17	0.138	0.667	0.053	0.696	0.250	0.386	0.017	0.020	0.101	0.007
0.016	980	0.120	7800	0.045	0.615	0.184	0.328	0.015	0.017	0.085	9000
0.012	0.000	880.0 60.0	0.490	0.036	0.515	0.122	0.264	0.012	0.013	0.067	0.005
2000	0.073	0.086	0.429	0.031	0.452	0.095	0.227	0.010	0.011	0.058	0.004
9000	0.062	0.070	0.352	0.025	0.372	0.067	0.184	0.008	0.009	0.046	0.003
3 8	0.053	0.060	0.305	0.022	0.322	0.053	0.158	0.007	0.008	0.039	0.003
9 8	0.043	0.048	0.244	0.017	0.258	0.039	0.125	0.006	900'0	0.031	0.002
500.0	0.036	0.040	0.205	0.014	0.217	0.031	0.105	0.005	0.005	0.026	0.002
3 8	0.028	0.031	0.158	0.011	0.167	0.023	0.080	0.004	0.004	0.020	0.001
7007	0.022	0.025	0.129	0.009	0.136	0.018	0.065	0.003	0.003	0.016	0.001
000	0.016	0.018	0.092	900:0	0.098	0.013	0.047	0.002	0.002	0.012	0.001



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										SUPCRIVO	1.000	0.988	0.670	200		0.276	0.158	0.041	0.032	0.029	0.027	0.025	0.024	0.023	0.022	0.021	0.021	0.020	0.020	0.019
										INFCRIVO	1.000	1.000	1.000	0 987	900	0.303	0.70	0.249	0.177	0.140	0.121	0.100	0.088	0.072	0.062	0.050	0.042	0.032	0.026	0.019
%0										ALMCRIVO	1.000	0.990	0.717	0.519	0.367	0.236	0.230	0.071	0.053	0.045	0.041	0.036	0.033	0.030	0.028	0.025	0.024	0.022	0.021	0.019
% E As2= 1		0.9801	0.1406	0.8395	46.22	49.23				SUPDORR	1.000	0.992	0.713	0.511	0.356	0.222	0.054	60.0	0.040	0.034	0.032	0.029	0.027	0.025	0.024	0.023	0.022	0.021	0.020	0.019
E As4 = 30		ALMCRI=	INFCRIVO	SUPCRIVO	RECIID 3.	6690	0.300	0.300		INFDORR	1.000	0.979	0.979	0.979	0.979	0.976	0 781		0.396	0.290	0.245	0.196	0.168	0.133	0.112	0.085	0.068	0.047	0.035	0.019
As1, As3		1.0887	0.1278	0.9609	76 49	m d.m	D503=	As3=		SUP 14	00.	0.932	0.932	0.932	0.932	0.932	0.932	0220	87/0	0.583	0.500	0.401	0.341	0.267	0.221	0.163	0.126	0.081	0.054	0.019
JLAÇÃO Nº 9 C/ m1 E m2 = 4, As1, As3 E As4 = 30% E As2= 10%		ALIM DORR=	INFDORR=	SUPDORR=	RECUP12n	2.099	0.040	0.008	INEAA"	4000	00.1 00.1	0.920	0.920	0.920	0.920	0.920	0.920	0.768	0.00	0.633	0.248	0.440	0.382	0.299	0.248	0.183	0.141	060.0	ecu.u	9.03
N° 9 C/ m	0.4607	6.1097	0.1505	0.0192	0.1505	m1=	D502=	As2=	SUP20"	500	8 6	0.990	0.744	0.565	0.429	0.310	0.140	0.082	0.064	0.057	800	0.04	\$ 00 C	0.038	0.034	0.030	770.0	0.024	0.022	90.0
SIMULAÇÃO	A! IM14"=		IN-14"	SUPRA14"	RP INFRA	2.095	0.100	0.300	INF20"	1,000	0.920	0200	0.920	0.920	0.920	0.920	0.920	0.761	0.626	0.542	0.440	0.376	0.295	0.245	0.180	3 5	50.00	0.000	0.019	
IS ·	1.268	0.4607	7507	1.0887	1.0887	m1=	D501=	As1=0	ALM20"	1.000	0.974	0.763	0.640	0.010	0.483	0.392	0.246	0.174	0.141	0.123	0.102	0.089	0.073	0.063	0.050	0.042	0.032	0.026	0.019	
į	ALM20"=	INFRA 20"=	- CACOLLA	SUPRAZU=	RP SUPRA	1	1		ALIM CIRC.	1.000	0.978	0.710	0.518	0.380	200	0.201	0.183	0.140	0.117	0.103	0.086	0.075	0.062	0.053	0.043	0.036	0.028	0.022	0.016	
									LUZ	6.000	4.000	2.000	1.000	0.500	0.250	0.074	* 0.00	0.048	0.032	0.024	0.016	0.012	0.008	0.006	0.004	0.003	0.002	0.002	0.001	

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				SIMULAÇA	O N° 10 C	MULAÇÃO N° 10 C/ D50 CICLONE DE 20" = 100 μm	NE DE 20	= 100 µm	E As1=30%	%		
NIFRA 20** 0.1421 NIF14** 0.1339 NIFRORNEA 0.06529 NIFRA 20** 0.1539 NIFRORNEA 0.06529 NIFRA 20** 0.1539 NIFRORNEA 0.06529 NIFRA 20** 0.1539 N		ALM20"	1.095	ALIM14"=	0.1421	AI IM DOOD.	0000					
SUPPRAZO** 0.0529 SUPPRA1*** 0.0029 SUPPRA1*** 0.0029 SUPPRA1*** 0.0029 SUPPRA1*** 0.0029 SUPPRA1*** 0.0029 SUPPRA1*** 0.0029 SUPPRA1** 0.0029 MIFE DEG1** 0.100 DEG2** 0.0029 MIFE 0.0029 0.002		INFRA 20"=	0.1421	INF14"=	0 1320	WEDGEN.	0.9529	ALMCRI=	0.8831			
RP SUPRA 1.0611 RP INFRA 0.1566 RECUP-121 5.48 RECUP-121 M11 2.065 m1 2.089 m1 0.653 RECUP-121 D501= 0.100 D502= 0.203 m1 0.623 0.630 A51=0 0.100 D502= 0.203 m1 0.630 0.630 A51=0 0.100 D502= 0.203 m1 0.630 0.630 0 1.000 1.000 1.000 1.000 1.000 1.000 1.000 0 0.070 1.000 1.000 1.000 1.000 1.000 1.000 0 0.071 0.072 1.001 0.974 1.000 1.000 1.000 0 0.073 0.048 1.000 1.000 1.000 1.000 1.000 0 0.580 0.429 1.001 0.046 0.000 1.000 1.000 1.000 0 0.518 0.525 1.001 0.022		SUPRA20"	0.9529	SUPRA14"=	00000	INTUOKKE THE PERSON	0.0688	INFCRIVO	0.026			
Mail		RP SUPRA	1.0611	S CONTROL	0.0082	SUPDORR=	0.8841	SUPCRIVO=	0.8571			
ALIMACIRC. ALIMZOT. D1502- 0.221 D503- m14- 0.023 D503- 0.023 D503- 0.030 AS1-0 0.100 D502- 0.221 D503- 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.000 0.300 0.000			1000	AF INFKA	0.1586	RECUP12µ	95.48	RECUP2µ	96.27			
ALIM CIRC. ALIM CI		-	E I	2.095	m1=	2.099	m1*	0.623				
Main Circ. ALIM Circ. ALIMZOT INFZOT INFACT INFORRA 1.000 1.00			D501=	0.100	D502=	0.221	D503=	0.300				
ALIM CIRC. ALMZO* INF2O* SUP2O* INF10* SUP14* SUP14* INFDORR 0 1,000 1,000 1,000 1,000 1,000 1,000 1,000 0 0.978 0.970 1,001 0.974 1,000 1,000 1,000 1,000 0 0.710 0.729 1,001 0.682 1,000 1,000 1,000 1,000 0 0.380 0.429 1,001 0.488 1,000 1,000 1,000 0 0.281 0.329 1,001 0.488 1,000 1,000 1,000 0 0.289 0.429 1,001 0.229 1,000 1,000 1,000 1,000 0 0.281 0.021 0.229 1,000 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289 0.289			As1=0	0.300	As2=	0.008	As3=	0.832				
ALIM CIRC. ALIM CIRC. ALIM CIRC. ALIM CIRC. INF20* SUP20* INF14* SUP14* INFDORR* INFDORR* 0 9978 1,000 1,000 1,000 1,000 1,000 1,000 1,000 0 9778 0,710 0,729 1,001 0,674 1,000 1,000 1,000 0 0,710 0,729 1,001 0,682 1,000 1,000 1,000 1,000 0 0,280 0,429 1,001 0,488 1,000 1,000 1,000 1,000 0 0,281 0,429 1,001 0,248 1,000 1,00			,									
0 1,000 1,0	LUZ	ALIM CIRC.	ALM20"	INF20"	SUP20"	INE 14"						
0 0.978 0.970 1.001 0.894 1.000 1.000 1.000 0 0.710 0.729 1.001 0.692 1.000 1.000 1.000 1.000 0 0.518 0.655 1.001 0.488 1.000 1.000 1.000 1.000 0 0.380 0.429 1.001 0.229 1.000 1.000 1.000 1.000 0 0.281 0.222 0.980 0.102 0.893 0.895 0.895 0.896 0.896 0.899 0.899 0.896 0.899 0.899 0.896 0.971 0.899 0.896 0.896 0.971 0.897 0.896 0.896 0.971 0.897 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.896 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996	000.9	1.000	1.000	1.000	1.000	100	100	INFLOORE	SUPDORR	ALMCRIVO	INFCRIVO	SUPCRIVO
0 710 0.728 1,001 0.692 1,000 1,000 1,000 0 518 0.555 1,001 0.682 1,000 1,000 1,000 0 380 0.429 1,001 0.488 1,000 1,000 1,000 0 281 0.281 1,001 0.229 1,000 0.999 0.995 4 0.183 0.222 0.880 0.102 0.991 0.892 0.995 8 0.140 0.172 0.814 0.071 0.837 0.466 0.546 9 0.117 0.141 0.865 0.054 0.711 0.446 0.546 1 0.102 0.865 0.046 0.630 0.213 0.446 0.539 0.213 0.446 0.539 0.713 0.224 0.213 1 0.103 0.102 0.506 0.046 0.639 0.136 0.136 0.214 0.224 0.239 0.141 1 0.043 0.043 0.043	4.000	0.978	0.970	1001	0.024	000:	00.	1.000	1.000	1.000	1.000	1,000
0 518 0.555 1,001 0,002 1,000 1,000 1,000 0 380 0,429 1,001 0,341 1,000 1,000 1,000 1,000 0 281 0,281 1,001 0,229 1,000 0,999 0,999 0,999 0,999 4 0,183 0,222 0,980 0,102 0,991 0,899 0,998	2.000	0.710	0.729	5	t 60.0	000.1	90.	1.000	0.972	0.972	1.000	0.971
0 380 0 429 1,001 0,341 1,000 <th< td=""><td>1.000</td><td>0.518</td><td>0.555</td><td>5 6</td><td>0.092</td><td>1.000</td><td>1.00</td><td>1.000</td><td>0.661</td><td>0.664</td><td>1,000</td><td>0.655</td></th<>	1.000	0.518	0.555	5 6	0.092	1.000	1.00	1.000	0.661	0.664	1,000	0.655
0 281 0.334 1,001 0.229 1,000 0,095 0,095 0,095 0,096 0,096 0,007 0,097 0,093 0,096 0,046 0,074 0,047 0,048 0,042 0,042 0,042 0,044 0,032 0,046 0,074 0,203 0,026 0,026 0,074 0,203 0,026 0,026 0,026 0,074 0,026 <th< td=""><td>0.500</td><td>0.380</td><td>0.429</td><td>8. 5</td><td>0.488</td><td>1.000</td><td>1.000</td><td>1.000</td><td>0.437</td><td>0.443</td><td>0.981</td><td>0.427</td></th<>	0.500	0.380	0.429	8. 5	0.488	1.000	1.000	1.000	0.437	0.443	0.981	0.427
4 0.163 0.222 0.980 0.123 1,000 0.999 0.995 8 0.140 0.172 0.980 0.102 0.991 0.802 0.818 9 0.140 0.172 0.814 0.071 0.837 0.446 0.546 1 0.103 0.123 0.056 0.054 0.711 0.274 0.421 1 0.086 0.102 0.506 0.046 0.630 0.203 0.236 0 0.086 0.102 0.506 0.036 0.036 0.136 0.251 0 0.052 0.074 0.035 0.046 0.050 0.174 0.251 0 0.053 0.056 0.253 0.048 0.043 0.174 0.203 0 0.043 0.050 0.253 0.016 0.026 0.043 0.116 0.026 0 0.036 0.042 0.014 0.012 0.026 0.043 0.116 0.026 0.043<	0.250	0.281	0.334	<u>.</u>	. c. c.	1.000	1.000	1.000	0.274	0.282	0.873	0.265
3 0.140 0.172 0.814 0.071 0.891 0.802 0.818 2 0.140 0.172 0.814 0.071 0.837 0.446 0.546 2 0.173 0.123 0.054 0.711 0.274 0.421 3 0.086 0.123 0.046 0.630 0.203 0.359 4 0.075 0.089 0.444 0.032 0.466 0.105 0.251 5 0.062 0.074 0.032 0.046 0.074 0.203 6 0.053 0.026 0.036 0.036 0.036 0.174 6 0.043 0.056 0.263 0.016 0.059 0.174 6 0.043 0.050 0.253 0.018 0.059 0.174 6 0.036 0.042 0.164 0.015 0.026 0.043 0.116 6 0.036 0.042 0.164 0.012 0.026 0.043 0.114	0.074	0.183	0.222	080	0.429	1.000	0.999	0.995	0.152	0.161	0.635	0.148
0.117 0.141 0.685 0.054 0.711 0.274 0.546 0.103 0.123 0.605 0.046 0.711 0.274 0.421 0.086 0.102 0.506 0.038 0.530 0.203 0.359 0.075 0.089 0.444 0.032 0.466 0.105 0.250 0.062 0.073 0.365 0.026 0.384 0.074 0.203 0.043 0.063 0.316 0.023 0.384 0.074 0.203 0.043 0.050 0.253 0.018 0.026 0.174 0.203 0.043 0.050 0.253 0.018 0.266 0.043 0.116 0.028 0.032 0.164 0.012 0.173 0.025 0.089 0.028 0.014 0.009 0.141 0.001 0.072 0.092 0.016 0.019 0.096 0.001 0.101 0.014 0.052 0.052	0.048	0.140	0.172	0.800	201.0	0.991	0.802	0.818	0.030	0.038	0.214	2 6 6
0.036 0.123 0.605 0.046 0.630 0.274 0.421 0.086 0.102 0.506 0.038 0.630 0.203 0.359 0.075 0.089 0.444 0.032 0.466 0.105 0.290 0.062 0.073 0.365 0.026 0.046 0.105 0.251 0.063 0.063 0.316 0.023 0.384 0.074 0.203 0.043 0.063 0.316 0.023 0.039 0.174 0.203 0.036 0.043 0.253 0.018 0.266 0.043 0.138 0.028 0.032 0.164 0.015 0.224 0.035 0.116 0.028 0.029 0.134 0.009 0.114 0.025 0.099 0.016 0.016 0.009 0.101 0.014 0.052 0.099	0.032	0.117	0.141	0.685	C.O.O.	0.837	0.446	0.546	0.023	0.027	0.157	0.024
0.086 0.102 0.506 0.038 0.530 0.203 0.359 0.075 0.089 0.444 0.032 0.66 0.105 0.290 0.062 0.073 0.026 0.034 0.074 0.251 0.063 0.063 0.316 0.026 0.384 0.074 0.203 0.043 0.050 0.253 0.018 0.059 0.174 0.203 0.036 0.042 0.213 0.018 0.266 0.043 0.136 0.028 0.032 0.164 0.012 0.173 0.025 0.089 0.028 0.032 0.134 0.095 0.141 0.020 0.072 0.016 0.019 0.096 0.007 0.101 0.014 0.052 0.052	0.024	0.103	0.123	0.605	500	U./1	0.274	0.421	0.017	0.020	0.119	0.017
0.075 0.089 0.44 0.032 0.466 0.136 0.290 0.062 0.073 0.365 0.026 0.384 0.074 0.251 0.053 0.063 0.316 0.023 0.333 0.059 0.174 0.043 0.050 0.253 0.018 0.266 0.043 0.174 0.036 0.042 0.213 0.015 0.026 0.043 0.116 0.028 0.032 0.134 0.015 0.017 0.016 0.016 0.017 0.026 0.089 0.028 0.036 0.036 0.037 0.096 0.141 0.020 0.072 0.052 0	0.016	0.086	0.102	0.508	2000	0.630	0.203	0.359	0.015	0.017	0.101	0.015
0.062 0.073 0.365 0.026 0.366 0.105 0.251 0.063 0.063 0.316 0.023 0.334 0.074 0.203 0.043 0.050 0.253 0.018 0.266 0.043 0.174 0.036 0.042 0.213 0.015 0.224 0.035 0.116 0.028 0.032 0.164 0.012 0.173 0.025 0.089 0.022 0.036 0.134 0.009 0.141 0.020 0.072 0.016 0.009 0.001 0.001 0.001 0.001 0.002	0.012	0.075	0.089	0.000	0000	0.530	0.136	0.290	0.012	0.013	0.080	0011
0.053 0.063 0.053 0.023 0.334 0.074 0.203 0.043 0.050 0.253 0.018 0.266 0.043 0.174 0.036 0.042 0.213 0.015 0.224 0.035 0.116 0.028 0.032 0.164 0.012 0.173 0.025 0.089 0.022 0.026 0.134 0.009 0.141 0.020 0.072 0.016 0.019 0.096 0.007 0.101 0.014 0.052	0.008	0.062	0.073	0.365	2000	0.466	0.105	0.251	0.010	0.011	690.0	0.010
0.043 0.050 0.253 0.018 0.256 0.059 0.174 0.036 0.042 0.213 0.015 0.224 0.035 0.116 0.028 0.032 0.164 0.012 0.173 0.025 0.089 0.022 0.026 0.134 0.009 0.141 0.020 0.072 0.016 0.019 0.096 0.007 0.101 0.014 0.052	9000	0.053	0.063	0.316	0.020	0.384	0.074	0.203	0.008	600.0	0.055	9000
0.036 0.042 0.213 0.015 0.224 0.035 0.116 0.028 0.032 0.164 0.012 0.173 0.025 0.089 0.022 0.026 0.134 0.009 0.141 0.020 0.072 0.016 0.019 0.096 0.007 0.101 0.014 0.052	0.004	0.043	0.050	0.253	0.02	0.333	0.059	0.174	0.007	0.008	0.047	0.007
0.028 0.032 0.164 0.012 0.173 0.025 0.089 0.022 0.026 0.134 0.009 0.141 0.020 0.072 0.016 0.019 0.096 0.007 0.101 0.014 0.052	0.003	0.036	0.042	0.213	0.015	0.200	0.043	0.138	900.0	900.0	0.037	0.005
0.022 0.026 0.134 0.009 0.141 0.020 0.072 0.016 0.096 0.007 0.101 0.014 0.052	0.002	0.028	0.032	0.164	0.012	0.224	0.035	0.116	0.005	0.005	0.031	0.004
0.016 . 0.019 0.096 0.007 0.101 0.014 0.052	0.002	0.022	0.026	0.134	6000	0.173	CZ0.0	0.089	0.004	0.004	0.024	0.003
70.0	0.001	0.016	. 0.019	960.0	0.007	0.101	0.020	0.072	0.003	0.003	0.019	0.003
							410.0	7cn:n	0.002	0.002	0.014	0.002

RESULTADOS DA OPTIMIZAÇÃO DE PARÂMETROS

			'	OLI COLO			
ALM20"=	1.289	ALIM14"=	0.1816	0.1816 ALIMDORR=	1.0974	ALMCRI"=	1.0016
SUPRA20"=	1.0974	1.0974 INFRA14"=	0.1431	INFDORR=	0.1343	SUPRACRIV	0.8469
INFRA 20"	0.1816	D.1816 SUPRA14"=	0.0385	0.0385 SUPRADORR	0.9632	INFCRIVO	0.1547

LUZmm	ALIM CIRC	ALM20"	INF20"	SUP20"	INF14"	SUP14"	INFDORR	SUPDORR	ALMCRIVO	INFCRIVO	INFCRIVO SUPCRIVO
6.000	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	8.
4.0000	96.0	0.97	1.00	0.98	1.00	1.80	1.00	76.0	96:0	1.00	76:0
2.0000	0.71	0.77	1.00	67.0	1.00	1.00	1.00	0.70	0.71	1.00	99.0
1.0000	0.52	0.62	1.00	0.56	1.00	1.00	1.00	0.49	0.51	0.39	0.43
0.5000	0.38	0.50	1.00	0.42	1.00	1.00	1.00	0.34	0.37	0.91	0.27
0.2500	0.28	0.40	1.00	0:30	1.00	1.00	1.00	0.21	0.24	0.73	0.15
0.0740	0.18	0.26	1.00	0.13	1.00	1.00	0.82	0.04	90.0	0.32	හ.0
0.0480	0.14	0.18	0.84	0.07	0.85	0.82	6,43	0.02	90'0	0.24	0.02
0.0320	0.12	0.15	0.71	90'0	0.72	0.68	0.32	0.02	9.0	0.19	0.02
0.0240	0.10	0.13	හ.0	90'0	හ.0	09:0	0.27	0.02	0.04 40.04	0.17	0.01
0.0160	0.09	0.11	0.52	0.04	0.53	05:0	0.22	0.01	9.03	0.14	0.01
0.0120	90:0	60:00	0.46	60.03	0.46	0.44	0.19	0.01	ഇ'0	0.12	0.01
0.0080	90.0	0.08	0.38	0.03	0.38	96.0	0.16	10.0	0.02	0.10	0.01
0.0060	90:0	0.07	0.33	0.02	0.33	0.31	0.14	0.01	0.02	60.0	0.01
0.0040	0.04	90.0	0.26	0.02	0.26	0.25	0.11	0.01	0.02	0.07	0.01
0.0030	0.04	0.04	0.22	0.02	0.22	0.21	60'0	0.01	10.0	90'0	0.00
0.0020	0.03	0.03	0.17	0.01	0.17	0.16	20'0	0.00	0.01	90:0	0.00
0.0015	0.02	0.03	0.14	0.01	0.14	0.13	90'0	0.00	10.0	0.04	0.00
0.0010	0.02	0.02	0.10	0.01	0.10	60:0	0.04	0.00	0.01	900	0.00

RESUMO

Este trabalho tem por objectivo o estudo critico e a avaliação da eficiência do circuito de classificação da instalação de tratamento de caulinos da Mina de Valverde, pertencente à Companhia Anglo Portuguesa de Caulinos de Viana, grupo English China Clay (ECC Ltd).

Devido às dificuldades encontradas em relação ao tratamento dos dados experimentais e à determinação dos parâmetros de cada classificador, resultantes principalmente do facto constatado de que nem o circuito nem os classificadores se encontravam em regime permanente, desenvolveu-se uma metodologia própria para a determinação dos parâmetros que modelam as curvas de partição dos classificadores e da avaliação global do desempenho do circuito.

Este método resulta ser de extrema utilidade sempre que nos encontramos em situações idênticas às encontradas neste trabalho, em que o regime de funcionamento se encontra afastada do estado permanente, dado que esta é uma das condições necessàrias para aplicação das metodologias existentes para a modelização de operações e de circuitos de tratamento de minérios.

Por último, realizaram-se algumas reflexões sobre a eficiência de cada classificador e propuseram-se alternativas às suas condições de funcionamento, efectuando a simulação do circuito para diferentes condições operatórias. Estas simulações permitiram propor algumas alterações a efectuar no circuito existente de modo a optimizar os seus resultados, principalmente em relação a aumentos da recuperação global do circuito e eventual melhoria da composição granulométrica do produto final.



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